

AD-A119 496

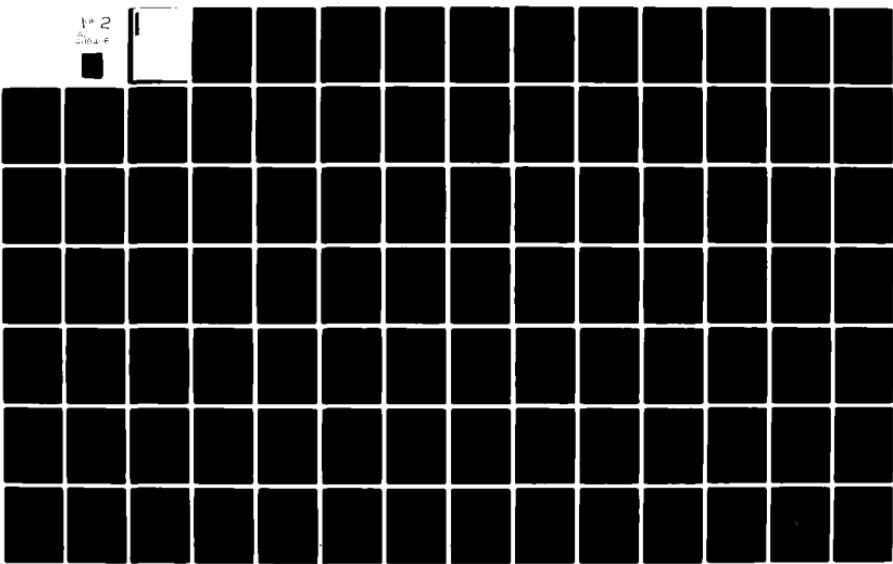
NAVAL SURFACE WEAPONS CENTER DAHLGREN VA
A METHOD TO CORRELATE THE UPPER AIR DENSITY WITH SURFACE DENSITY--ETC(U)
JUL 82 L J MCANELLY
NSWC/TR-82-81

F/6 4/1

NL

UNCLASSIFIED

1# 2
2004 P



AD A119496

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NSWC TR 82-81	2. GOVT ACCESSION NO. <i>AD-A119496</i>	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) A METHOD TO CORRELATE THE UPPER AIR DENSITY WITH SURFACE DENSITY AND ESTIMATE THE BALLISTIC DENSITY FOR AIR OR SURFACE LAUNCHED MISSILES	5. TYPE OF REPORT & PERIOD COVERED Final	
7. AUTHOR(s) Loren J. McAnelly	6. CONTRACT OR GRANT NUMBER(s)	
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Surface Weapons Center (K11) Dahlgren, VA 22448	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS SF 32-391-694 SF 32-399-694	
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Surface Weapons Center Dahlgren, VA 22448	12. REPORT DATE July 1982	
14. MONITORING AGENCY NAME & ADDRESS(if different from Controlling Office)	13. NUMBER OF PAGES 117	
	15. SECURITY CLASS. (of this report) UNCLASSIFIED	
	15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES <i>A</i>		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Atmospheric density Ballistic density Exponential functions of altitude Least-squares technique Nomograms		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Atmospheric data collected twice daily from five ocean stations over a period of 7 years were used in a study to correlate ballistic densities at various levels. The study indicates that a good correlation does exist and that tables, nomograms, or data in a suitable format should be produced for use with new and existing fire control computers and range tables prepared for the Fleet.		

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

20. ABSTRACT (Cont.)

Two exponential functions of altitude were used to express the density—one from surface to 36,000 ft, the other from 36,000 to 65,000 ft. The coefficients were selected in a manner that produces a continuous function from sea level to 65,000 ft. The coefficients of the two functions were determined using a non-linear least-squares technique.

Fluctuations in the density profiles below 5,000 ft altitude were noted and were investigated by fitting a sample of temperature and pressure data with a least-squares technique.

Ballistic densities for firing at surface targets were computed for altitudes to 50,000 ft. While the current projectiles in the Fleet may not reach an altitude of 50,000 ft, this may become a reality in the near future. The procedure presented in this report could very easily be modified to compute ballistic density when firing at air targets at altitudes up to 50,000 ft.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

TR 82-81

FOREWORD

The range tables for Navy guns include a nomogram for computing ballistic density, which may be used when only the surface density is known. While these nomograms are intended for use when better estimates of ballistic density are not available, they are based on data prepared in 1922, despite the advent of radiosondes and the establishment of ocean weather stations.

Since there frequently are times when a radiosonde observation cannot be made in the immediate operating area just before firing, or a timely and applicable meteorological message from the Fleet Numerical Weather Center (FNWC) is not available, another method for obtaining ballistic densities would serve a useful purpose.

This report documents a study that shows that ballistic densities can be estimated from the surface density with a reasonable degree of accuracy. Data are also presented about the upper atmosphere which may be useful when further studies pertaining to the atmosphere are conducted.

The study was funded by the Naval Sea Systems Command Surface Weapons Aerodynamics and Structures Research and Development Block Program.

Released by:

O. F. Braxton

O. F. BRAXTON, Head

Strategic Systems Department

iii



A

TR 82-81

ACKNOWLEDGEMENT

The author would like to thank Dr. W. A. Kemper and Mr. Henry E. Castro for their help in preparing this report. Dr. Kemper provided valuable assistance in preparing the text of this report. Mr. Castro derived a nonlinear least-squares technique which was used to fit the observed density data. The technique is described in Appendix A.

TR 82-81

CONTENTS

	<u>Page</u>
INTRODUCTION.....	1
DETAILED PROCEDURE.....	4
FITTING A SAMPLE SET OF DATA WITH AN ALTERNATE PROCEDURE.....	7
FITTING THE U.S. STANDARD ATMOSPHERE.....	9
RESULTS.....	13
DISCUSSION OF RESULTS.....	14
CONCLUSIONS.....	17
RECOMMENDATIONS.....	18
REFERENCES.....	19
APPENDIX A - A NONLINEAR LEAST-SQUARES TECHNIQUE.....	A-1
APPENDIX B - AN ALTERNATE METHOD FOR COMPUTING DENSITY.....	B-1
APPENDIX C - COEFFICIENTS OBTAINED BY FITTING OBSERVED DENSITY	C-1
APPENDIX D - DENSITY RATIO PROFILES FOR STATION E.....	D-1
APPENDIX E - BALLISTIC DENSITY PROFILES FOR STATION E.....	E-1
APPENDIX F - SELECTED BALLISTIC DENSITIES FOR STATIONS E, V, D, N, AND C.....	F-1
DISTRIBUTION.....	(1)

INTRODUCTION

One of the basic premises of fire control systems in use in the Fleet today is a "Standard Atmosphere." Obviously, the same premise is also used in the preparation of ballistic tables for the Fleet. Since the conditions used as a basis for a standard atmosphere are rarely encountered on earth, corrections for nonstandard conditions are always in order. A procedure frequently used to correct for a non-standard density involves a ballistic air density in the solution of fire control problems. The ballistic air density may be defined as a scale factor that, when multiplied by the standard air density at each altitude, produces a density structure that would cause the same displacement of a projectile impact point as the actual density structure.

The most reliable method of determining ballistic density is to use accurate, representative, and timely meteorological observations in the computation. There are, however, occasions when these measurements are not available, and alternate methods are necessary to provide the requisite information. It is a standard procedure to include a nomogram in the ballistic tables for the Fleet. The use of the nomogram is an alternative that is available to the Fleet for estimating the upper air density for naval gunfire when a ballistic meteorological forecast is not available. The nomograms may be used to estimate the ballistic density when the air temperature, pressure, and relative humidity at the surface are known.

The basic data used to prepare the nomograms were obtained from Table IV, The Ballistic Density Factor,¹ which was published in 1935. A footnote to this table states, "This table has been extracted from Table C of a pamphlet entitled Method for Determining Air Temperature and Ballistic Air Density, published by the Signal Corps (Meteorological Service), U.S. Army in 1922."

Fire control systems have been improved to the point where an accurate determination of the upper air density is required if the potential of the systems is to be fully utilized. The need for improving the nomograms or providing an alternate procedure to determine the ballistic density has long been recognized.

The work described in this report, stated briefly, consisted of (1) obtaining Rawinsonde data from various weather stations, (2) sorting the data according to

surface densities and seasons, (3) fitting the upper air densities with a least-squares technique, and (4) computing ballistic densities.

Rawinsonde data used in the study were obtained from five maritime stations which took soundings daily at 0000 and 1200 hr G.m.t. over a period from 1968 to 1973. The data, consisting of both significant and mandatory levels, were provided by the National Climatic Center, Asheville, North Carolina. Mandatory levels are specified pressure altitudes, which are obtained by interpolation. Significant levels are the altitudes that are considered essential in defining a weather profile. Soundings that did not include surface density were not used in the study. Some of the obvious errors were eliminated in processing the data prior to performing the least-squares fit, but no attempt was made to eliminate errors in the basic data beyond that point.

The geodetic coordinates of the five stations used in the study are listed below:

<u>Station Name</u>	<u>Latitude</u>	<u>Longitude</u>
E	35° 0' N	48° 0' W
V	34° 0' N	164° 0' E
C	52° 45' N	35° 30' W
D	44° 0' N	41° 0' W
N	30° 0' N	140° 0' W

A map of the stations is shown in Figure 1.

No land-based stations were used in the analysis, even though naval gunfire support is conducted on beach areas. Since the density correlations are markedly affected by the nature of the terrain,² there is more than a probability that somewhat different results would be obtained for different littoral areas of the earth.

All computer programs used in the study were coded in FORTRAN EXTENDED and were executed with a Control Data Corporation (CDC) 6700 computer.

The purpose of performing the work described in this report was to establish a procedure to determine the correlation between upper air and surface densities and

TR 82-81

LOCATION OF WEATHER STATIONS

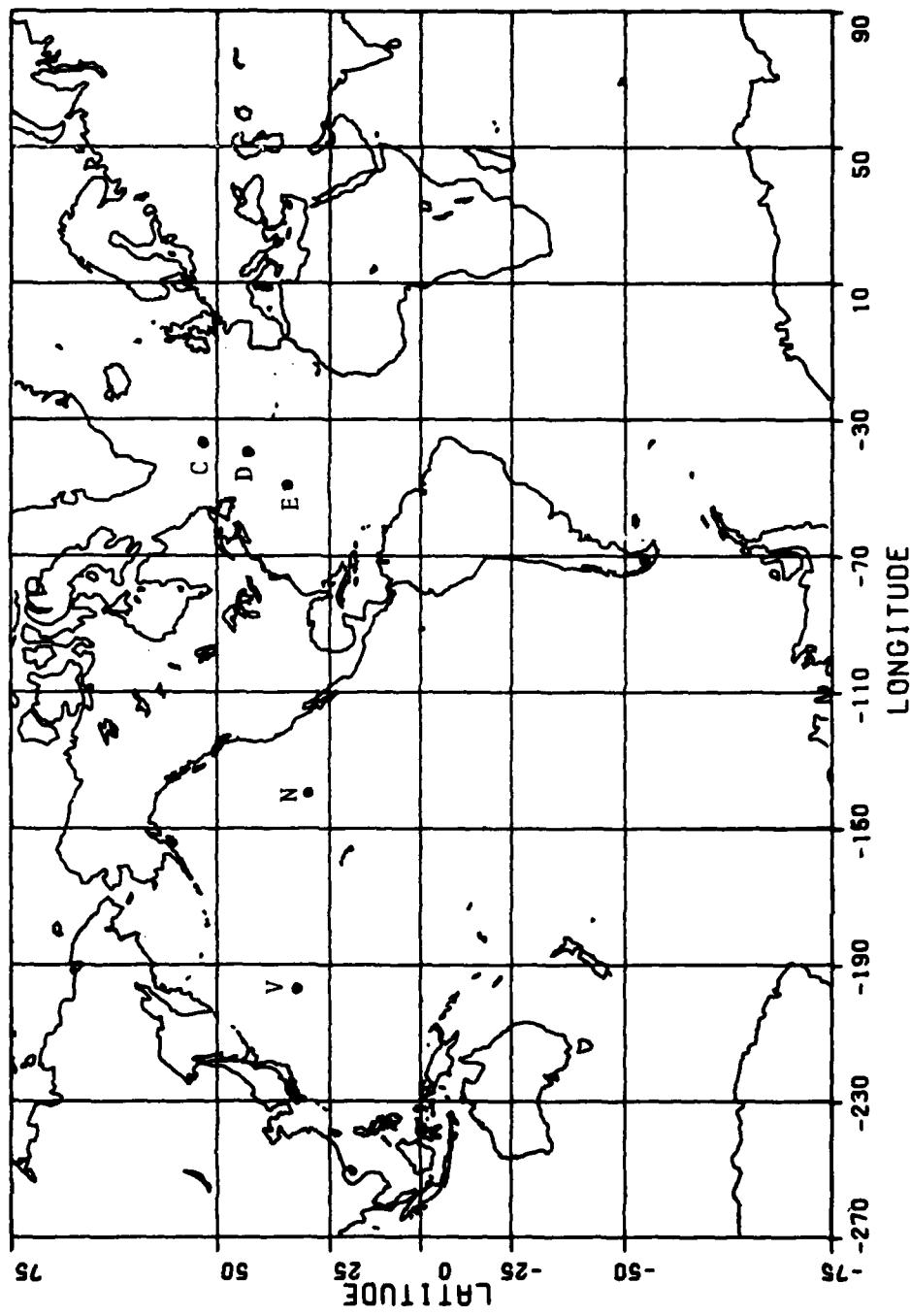


FIGURE 1. MAP OF STATIONS USED IN THE STUDY

to devise a method for estimating the ballistic air density based on surface conditions.

DETAILED PROCEDURE

The first step in the procedure was to compute the air density using the temperature, pressure, and relative humidity. The geopotential altitudes were converted to geometric altitudes. Sondes that did not include surface conditions were omitted. The data for each station were sorted into two groups according to the time of day and stored in permanent files with the Indexed-Sequential File Organization. This procedure permits accessing the data in either a sequential or random order. The sondes were assigned indices which were stored in separate sequential files. One file of indices was created with the corresponding surface densities in ascending numerical order, and a second file was created with the surface densities also sorted into the four seasons. A follow-up program was designed to skip specified segments when the files were read. This made it convenient to group the data in various ways without rearranging the Indexed-Sequential files.

The data were then selected in groups where the median surface density of each group varied by a percentage point from the U.S. Standard surface density as defined in Reference 3 (i.e., into classes by surface density ratios where the class interval was one percent). Since large variations were encountered in the frequency of the surface densities, it was necessary to eliminate some of the sondes in the mid-ranges. Several fits were made using various numbers of samples in each fit. No significant differences were obtained by using more than 25 samples; consequently, a further restriction was placed on each group that limited the number of sondes to 25. While some of the groups outside the mid-ranges had variations in surface densities of one percent, the actual number of samples was, in some cases, less than 25. In contrast, some of the groups of 25 samples in the mid-ranges had variations in surface densities of only a fraction of one percent.

Various functions were investigated to represent a mean density profile for each group of data. Comparisons were made of three different functions for representing the density in the altitude range from 0 to 36,089 ft:

1. a third-degree polynomial
2. a third-degree polynomial for the ratio of the observed density to the U.S. Standard density
3. an exponential function plus a linear term

While these three functions produced similar results, the exponential function was selected. The fitting technique is described in Appendix A. The following expression was used in the altitude range from 0 to 36,089 ft:

$$\rho = c_1 e^{(c_2 h)} + c_3 h \quad (1)$$

where,

ρ is the density (lb/ft^3)

h is the altitude (ft)

c_1 , c_2 , and c_3 are constants determined by the fit

A similar expression was used to fit the data in the region from 36,089- to 65,000-ft altitude:

$$\rho = \rho_{36089} e^{(c_4 * (h - 36089))} + c_5 * (h - 36089) \quad (2)$$

where,

ρ_{36089} is the density at 36,089 ft, computed using equation (1) and the data up to 36,089 ft

c_4 and c_5 are coefficients determined in the fit above 36,089 ft

A bias was noted in the lower altitudes with each of the three methods. After some experimenting, data below 3,500 ft were excluded from the fit to determine the coefficients. The fit was then extrapolated to mean sea level, and a linear correction was added from 0 to 3,500 ft, which made ρ equal to ρ_0 at the surface:

TR 82-81

$$\rho = c_1 e^{(c_2 h)} + c_3 h + (\rho_0 - c_1)(3500 - h)/3500 \quad (3)$$

where,

ρ is the density (lb/ft^3)

c_1 , c_2 , and c_3 are the coefficients obtained with equation (1)

h is the altitude (ft)

ρ_0 is the median of the observed surface densities (lb/ft^3)

Although this procedure does not use any of the available data between surface and 3,500 ft in the least-squares fit to determine the coefficients c_1 , c_2 , and c_3 , residuals from the fit in this region are included in the analysis. Adding the linear correction made a significant improvement in the residuals from surface to 3,500 ft.

The upper boundary of 36,089 ft was selected from the zone where equation (1) was used in order to coincide with the breakpoint in the U.S. Standard atmosphere. While there are some seasonal, latitudinal, and diurnal variations in the isopycnic level where the density remains nearly constant, no attempt was made to explore this facet.

After fitting the observed density data, using equations (1) and (2), density profiles were computed using equations (2) and (3) with the coefficients obtained in the least-squares fit. Ballistic densities for each profile were computed with the equation,

$$\text{Ballistic Density} = \sum_{i=1}^n (WF_i * R_i) \quad (4)$$

where,

n is the number of zones

WF_i is the density weighting factor for the i th zone

R_i is the ratio of the mean density of the i th zone of the profile to the U.S. Standard density at that altitude, which is the mid-point of the i th zone.

The density weighting factors used to compute the ballistic density were obtained by computing trajectories with ballistic parameters for the 5-Inch High Fragmentation Projectile fired with a Mk 73 charge, which produces an initial velocity of 2,950 ft/sec. The altitudes covered by each zone are presented in Table 1, and a tabulation of the weighting factors are presented in Table 2.

TABLE 1. ALTITUDE OF ZONES

<u>Zone</u>	<u>Altitude (ft)</u>	<u>Zone</u>	<u>Altitude (ft)</u>	<u>Zone</u>	<u>Altitude (ft)</u>
1	0 - 1,000	10	9,000 - 10,000	19	26,000 - 28,000
2	1,000 - 2,000	11	10,000 - 12,000	20	28,000 - 30,000
3	2,000 - 3,000	12	12,000 - 14,000	21	30,000 - 32,000
4	3,000 - 4,000	13	14,000 - 16,000	22	32,000 - 34,000
5	4,000 - 5,000	14	16,000 - 18,000	23	34,000 - 36,000
6	5,000 - 6,000	15	18,000 - 20,000	24	36,000 - 38,000
7	6,000 - 7,000	16	20,000 - 22,000	25	38,000 - 40,000
8	7,000 - 8,000	17	22,000 - 24,000	26	40,000 - 45,000
9	8,000 - 9,000	18	24,000 - 26,000	27	45,000 - 50,000

FITTING A SAMPLE SET OF DATA WITH AN ALTERNATE PROCEDURE

An alternate method was used to fit a sample set of data in the region from surface to 36,000 ft. In this procedure, the virtual temperature was computed, using the observed temperature and relative humidity. Separate least-squares fits were then made to the virtual temperatures and pressures. The temperature and pressure profiles obtained in this manner were then used to compute the density. This procedure and the results are described in detail in Appendix B. The sample set of data was obtained from 25 sondes that had been selected previously for fitting with equation (1). The sondes were observed at Station E during the spring season, 1200 hr G.m.t., on days that had a surface density close to the U.S. Standard density at mean sea level.

TABLE 2. DENSITY WEIGHTING FACTORS

ZONES	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	
1	1.000																											
2	0.375	0.625																										
3	0.251	0.265	0.485																									
4	0.192	0.194	0.210	0.404																								
5	0.159	0.157	0.159	0.176	0.349																							
6	0.138	0.135	0.134	0.136	0.151	0.307																						
7	0.122	0.119	0.118	0.117	0.119	0.133	0.272																					
8	0.111	0.108	0.105	0.104	0.104	0.104	0.106	0.117	0.244																			
9	0.102	0.099	0.097	0.095	0.095	0.095	0.095	0.099	0.106	0.220																		
10	0.095	0.092	0.090	0.087	0.086	0.085	0.085	0.084	0.087	0.096	0.200																	
11	0.084	0.081	0.079	0.077	0.075	0.075	0.073	0.072	0.071	0.070	0.247																	
12	0.075	0.074	0.071	0.069	0.067	0.065	0.064	0.062	0.061	0.060	0.122	0.210																
13	0.069	0.067	0.065	0.063	0.063	0.062	0.060	0.058	0.056	0.055	0.105	0.106	0.180															
14	0.065	0.063	0.061	0.059	0.059	0.057	0.055	0.054	0.052	0.050	0.050	0.047	0.046	0.098	0.095	0.091	0.093	0.156										
15	0.061	0.059	0.057	0.055	0.053	0.053	0.052	0.050	0.049	0.047	0.047	0.046	0.046	0.098	0.095	0.091	0.092	0.135										
16	0.057	0.056	0.054	0.052	0.050	0.049	0.048	0.046	0.045	0.045	0.045	0.045	0.045	0.083	0.078	0.074	0.074	0.127	0.175	0.119								
17	0.053	0.053	0.051	0.050	0.048	0.047	0.045	0.044	0.042	0.041	0.079	0.074	0.104	0.070	0.067	0.064	0.065	0.104										
18	0.052	0.051	0.049	0.048	0.046	0.044	0.044	0.042	0.040	0.040	0.075	0.071	0.106	0.063	0.060	0.058	0.058	0.091										
19	0.050	0.049	0.047	0.045	0.044	0.043	0.041	0.040	0.039	0.038	0.072	0.068	0.065	0.061	0.059	0.055	0.053	0.052	0.079									
20	0.048	0.047	0.045	0.044	0.042	0.041	0.040	0.039	0.037	0.037	0.059	0.060	0.062	0.058	0.056	0.053	0.051	0.051	0.048	0.047	0.047	0.045	0.043	0.043	0.060			
21	0.047	0.045	0.044	0.042	0.041	0.040	0.039	0.038	0.036	0.035	0.067	0.063	0.060	0.056	0.053	0.050	0.049	0.047	0.047	0.047	0.045	0.043	0.043	0.042	0.039	0.051		
22	0.046	0.044	0.043	0.041	0.040	0.039	0.038	0.037	0.035	0.034	0.065	0.061	0.057	0.054	0.051	0.048	0.046	0.043	0.043	0.042	0.042	0.042	0.042	0.040	0.036	0.046		
23	0.045	0.044	0.042	0.041	0.039	0.038	0.037	0.036	0.034	0.033	0.064	0.060	0.055	0.053	0.049	0.046	0.043	0.042	0.042	0.040	0.038	0.037	0.036	0.035	0.034	0.035		
24	0.044	0.043	0.042	0.040	0.039	0.038	0.037	0.036	0.034	0.034	0.059	0.059	0.057	0.052	0.048	0.045	0.042	0.040	0.037	0.035	0.034	0.034	0.033	0.032	0.031	0.031		
25	0.043	0.042	0.041	0.040	0.038	0.037	0.036	0.034	0.034	0.032	0.062	0.058	0.054	0.050	0.047	0.044	0.041	0.039	0.036	0.034	0.033	0.032	0.031	0.028	0.026	0.025		
26	0.042	0.041	0.039	0.037	0.037	0.036	0.035	0.035	0.033	0.032	0.031	0.059	0.056	0.053	0.049	0.045	0.043	0.039	0.037	0.035	0.032	0.031	0.028	0.026	0.025	0.029		
27	0.041	0.040	0.039	0.037	0.036	0.035	0.034	0.034	0.033	0.032	0.030	0.059	0.055	0.051	0.047	0.044	0.042	0.038	0.037	0.034	0.032	0.029	0.027	0.025	0.024	0.023	0.027	

The purpose of using the alternate method was to evaluate the method described in the section Procedure and to provide additional information about the atmosphere, particularly in the lower altitudes.

While this method is a good procedure for providing temperature, pressure, and density profiles, it is a more time-consuming method for obtaining density profiles than the method of making a least-squares fit to the densities.

The density profile obtained with this method did not result in a noticeably different profile, but it did provide additional information about the temperature and pressure. The pressure data from surface to 36,000-ft altitude were fit with a single function that has a continuous derivative. The temperature data were divided into three altitude zones. Separate least-squares fits were made to each zone in a manner that made the curve continuous but with a different lapse rate in each zone. The improvement in using the correction term in equation (3) to fit the density is largely due to the variations in the temperature lapse rate at the lower altitudes.

FITTING THE U.S. STANDARD ATMOSPHERE

In order to further test the least-squares method and the exponential representation of the density, a fit was made to the U.S. Standard density, using equations (1) and (2). Since the U.S. Standard temperature has a constant lapse rate from surface to 36,089-ft altitude, the correction term in equation (3) was not used. It should be noted that equations (1) and (2) were not intended to define the U.S. Standard density but were selected to fit the observed data. However, the standard deviations in the fit were only 0.14 and 0.28 percent in the zones from 0- to 36,089-ft, and 36,089- to 65,000-ft altitude, respectively. Since the density varies with altitude, the residuals were expressed as ratios of the U.S. Standard density at the corresponding altitude. A tabulation of the fit is presented in Tables 3 and 4.

TABLE 3. LEAST-SQUARES FIT OF U.S. STANDARD DENSITY
0 - 36,000 ft

1 Altitude (ft)	2 U.S. Standard Density (1b/ft ³)	3 L. S. Fit Density (1b/ft ³)	4 Col. 2 - Col. 3 Col. 3
0.	0.076474	0.07665845	-0.00240610
500.	0.075362	0.07551388	-0.00201122
1,000.	0.074262	0.07438439	-0.00164533
1,500.	0.073174	0.07326977	-0.00130712
2,000.	0.072098	0.07216982	-0.00099517
2,500.	0.071035	0.07108433	-0.00069395
3,000.	0.069984	0.07001309	-0.00041553
3,500.	0.068945	0.06895591	-0.00015824
4,000.	0.067917	0.06791259	0.00006494
4,500.	0.066902	0.06688293	0.00028510
5,000.	0.065898	0.06586675	0.00047450
5,500.	0.064906	0.06486384	0.00064991
6,000.	0.063925	0.06387404	0.00079783
6,500.	0.062956	0.06289715	0.00093568
7,000.	0.061998	0.06193299	0.00104969
7,500.	0.061051	0.06098138	0.00114159
8,000.	0.060116	0.06004216	0.00122986
8,500.	0.059191	0.05911513	0.00128338
9,000.	0.058278	0.05820014	0.00133776
9,500.	0.057375	0.05729702	0.00136106
10,000.	0.056483	0.05640559	0.00137245
10,500.	0.055602	0.05552569	0.00137431
11,000.	0.054731	0.05465717	0.00135085
11,500.	0.053871	0.05379985	0.00132241
12,000.	0.053022	0.05295360	0.00129174
12,500.	0.052182	0.05211824	0.00122336
13,000.	0.051353	0.05129363	0.00115745
13,500.	0.050534	0.05047962	0.00107734
14,000.	0.049725	0.04967605	0.00098539
14,500.	0.048926	0.04888278	0.00088407
15,000.	0.048137	0.04809968	0.00077598
15,500.	0.047358	0.04732658	0.00066389
16,000.	0.046589	0.04656336	0.00055067
16,500.	0.045829	0.04580987	0.00041754
17,000.	0.045079	0.04506598	0.00028881
17,500.	0.044338	0.04433156	0.00014526
18,000.	0.043606	0.04360647	-0.00001072
18,500.	0.042884	0.04289057	-0.00015329

TR 82-81

TABLE 3. LEAST-SQUARES FIT OF U.S. STANDARD DENSITY
0 - 36,000 ft (Continued)

1 Altitude (ft)	2 U.S. Standard Density (lb/ft ³)	3 L. S. Fit Density (lb/ft ³)	4 <u>Col. 2 - Col. 3</u> Col. 3
19,000.	0.042171	0.04218375	-0.00030232
19,500.	0.041468	0.04148588	-0.00043087
20,000.	0.040773	0.04079682	-0.00058376
20,500.	0.040087	0.04011645	-0.00073413
21,000.	0.039410	0.03944466	-0.00087867
21,500.	0.038742	0.03878132	-0.00101387
22,000.	0.038083	0.03812631	-0.00113606
22,500.	0.037432	0.03747953	-0.00126803
23,000.	0.036790	0.03684084	-0.00137995
23,500.	0.036156	0.03621014	-0.00149516
24,000.	0.035531	0.03558732	-0.00158251
24,500.	0.034914	0.03497226	-0.00166590
25,000.	0.034306	0.03436486	-0.00171279
25,500.	0.033705	0.03376501	-0.00177724
26,000.	0.033113	0.03317260	-0.00179668
26,500.	0.032529	0.03258753	-0.00179614
27,000.	0.031952	0.03200970	-0.00180254
27,500.	0.031384	0.03143900	-0.00174942
28,000.	0.030823	0.03087534	-0.00169508
28,500.	0.030270	0.03031861	-0.00160323
29,000.	0.029725	0.02976872	-0.00146858
29,500.	0.029187	0.02922557	-0.00131974
30,000.	0.028657	0.02868907	-0.00111786
30,500.	0.028134	0.02815913	-0.00089227
31,000.	0.027619	0.02763564	-0.00060224
31,500.	0.027110	0.02711853	-0.00031466
32,000.	0.026610	0.02660771	0.00008623
32,500.	0.026116	0.02610307	0.00049524
33,000.	0.025629	0.02560455	0.00095501
33,500.	0.025149	0.02511204	0.00147165
34,000.	0.024676	0.02462548	0.00205161
34,500.	0.024210	0.02414477	0.00270177
35,000.	0.023751	0.02366983	0.00342940
36,000.	0.022853	0.02273694	0.00510442

Mean of Column 4 -0.00000178

Standard Deviation of Column 4 0.00140643

TR 82-81

TABLE 4. LEAST-SQUARES FIT OF U.S. STANDARD DENSITY
36,200 - 65,000 ft

1 <u>Altitude</u> <u>(ft)</u>	2 <u>U.S. Standard Density</u> <u>(lb/ft³)</u>	3 <u>L. S. Fit Density</u> <u>(lb/ft³)</u>	4 <u>Col. 2 - Col. 3</u> <u>Col. 3</u>
36200.	0.022666	0.02253574	0.00578032
37000.	0.021814	0.02169457	0.00550490
38000.	0.020794	0.02068713	0.00516582
39000.	0.019822	0.01972648	0.00484233
40000.	0.018895	0.01881043	0.00449577
41000.	0.018012	0.01793693	0.00418541
42000.	0.017170	0.01710398	0.00385968
43000.	0.016367	0.01630972	0.00351190
44000.	0.015602	0.01555234	0.00319287
45000.	0.014873	0.01483014	0.00289033
46000.	0.014178	0.01414147	0.00258344
47000.	0.013516	0.01348478	0.00231541
48000.	0.012884	0.01285858	0.00197664
49000.	0.012282	0.01226147	0.00167447
50000.	0.011709	0.01169208	0.00144691
51000.	0.011162	0.01114914	0.00115366
52000.	0.010641	0.01063141	0.00090240
53000.	0.010144	0.01013772	0.00061976
54000.	0.0096701	0.00966695	0.00032545
55000.	0.0092186	0.00921805	0.00005944
56000.	0.0087882	0.00879000	-0.00020437
57000.	0.0083780	0.00838182	-0.00045561
58000.	0.0079870	0.00799260	-0.00070018
59000.	0.0076142	0.00762145	-0.00095105
60000.	0.0072589	0.00726754	-0.00118830
61000.	0.0069202	0.00693006	-0.00142260
62000.	0.0065973	0.00660825	-0.00165751
63000.	0.0062895	0.00630139	-0.00188719
64000.	0.0059961	0.00600878	-0.00211035
65000.	0.0057164	0.00572976	-0.00233130
Mean of Column 4		0.00003016	
Standard Deviation of Column 4		0.00284086	

The following equations were used in the least-squares fit of the U.S. Standard density:

$$0 \leq h \leq 36089$$

$$\rho = c_1 e^{(c_2 h)} + c_3 h$$

$$36,089 \leq h \leq 65,000$$

$$\rho = \rho_{36089} e^{(c_4 * (h - 36089))} + c_5 * (h - 36089)$$

where

h is the altitude (ft)

The coefficients obtained in the least-squares fit are:

$$\begin{aligned} c_1 &= 0.0766584476 \text{ (lb/ft}^3\text{)} \\ c_2 &= -0.282539693789 \text{ E-4 (ft}^{-1}\text{)} \\ c_3 &= -0.138466611596 \text{ E-6 (lb/ft}^4\text{)} \\ \rho_{36089} &= 0.0226549960 \text{ (lb/ft}^3\text{)} \\ c_4 &= -0.475504250122 \text{ E-4 (ft}^{-1}\text{)} \\ c_5 &= 0.459663274698 \text{ E-11 (lb/ft}^3\text{)} \end{aligned}$$

RESULTS

The coefficients that were obtained by fitting the density data, and the root mean squares (rms) or standard deviation of the residuals and their algebraic means are given in Appendix C for the five stations analyzed. Data are presented for two times of day (0000 and 1200 hr G.m.t.) for the four seasons and for the seasons combined for each station.

Profiles of the density ratios for station E are given in Appendix D. The ratios were obtained by evaluating the least-squares fit of the observed densities at specified altitudes and dividing the density in each case by the U.S. Standard

density for the same altitude. Profiles are shown for the two times of day for each of the four seasons and for the seasons combined.

Profiles of the ballistic densities obtained by multiplying the ratios with the density weighting factors using equation (4) are shown in Appendix E for station E for the same conditions. Density ratios and ballistic densities were computed for each of the five stations, but the profiles are shown only for station E in Appendixes D and E.

While the ballistic densities were computed for the 27 zones listed in Table 1, only an abbreviated tabulation is given in Appendix F. Data are presented for only two zones, 30,000 and 50,000 ft. The ballistic densities were computed with equation (4), using the density weighting factors given in Table 2. Data for the two zones are given for each of the five stations and for each surface condition where sufficient data were available to make a least-squares fit to the observed data.

DISCUSSION OF RESULTS

One question is of primary interest—is there sufficient correlation between surface density and that of the upper atmosphere to accurately predict the ballistic density for various altitudes from surface measurements? To answer this question, we first note that the density ratio curves given in Appendix D for station E are families of very similar curves. If some of the curves were missing, we could do a fair job of reproducing the curves by interpolation. This would seem to indicate, qualitatively at least, that one could predict the density ratios aloft from the starting point of the curve on the x-axis, which is the surface density ratio. The same is true of the curves given for ballistic density in Appendix E. It deserves mentioning that the points plotted in Appendix D are not the mean values of individual sondes but are values corresponding to the functional fit.

The sondes were grouped in order that a more reliable mean and standard deviation could be established. It is recognized that the curves in Appendix D do not reflect the errors of the means or the variations in the upper atmosphere within a

TR 82-81

group of sondes. A total of 14,800 sondes were processed in this study in an attempt to establish reliable means and standard deviations. In every fit, the mean and standard deviation were computed. These are tabulated in Appendix C. A large majority of the means are only a small fraction of one percent.

The standard deviations of the residuals are given in Table 5 according to percentiles. A total of 300 fits was made in each of the two altitude zones, 0 to 36,000 and 36,000 to 65,000 ft. The standard deviations of the residuals were arranged in numerical order without regard to station, season, or time of day. The standard deviation of the 50th percentile is 1.114 percent in the lower altitude zone.

TABLE 5. STANDARD DEVIATIONS OF THE RESIDUALS

<u>Percentile</u>	Altitude 0 - 36,000 (ft) (%)	Altitude 36,000 - 65,000 (ft) (%)
10	0.675	2.019
20	0.799	2.293
30	0.908	2.586
40	1.000	2.832
50	1.114	3.067
60	1.227	3.295
70	1.424	3.584
80	1.577	3.959
90	1.703	4.298
100	2.257	6.377

Note: The standard deviations in this table were obtained by multiplying the standard deviations (SIGMA) in Appendix C by 100 in order to express them as a percentage instead of as a ratio.

It should also be remembered that there are variations in the surface densities because of grouping the data, which probably has a negligible effect on the means but makes a small contribution to the standard deviations. The noise level in the data appears to increase with altitude, which is to be expected. The residuals are much larger in the fits above 36,000 ft than they are at the lower altitudes, while the density should be more stable at the higher altitudes.

It may be noted that the ballistic density represents a weighted average of the density ratios. Accordingly, any fluctuations that are random, and that may be

present in the ratios of the true density to the mean density, would tend to average out in computing the ballistic density.

Another question that deserves consideration is—how important is geographic location, season, and time of day? Only five stations used in the study are located in wide ocean areas, far from land, and between 30° and 50° N latitude. Data were available for only two times of day, 0000 and 1200 hr G.m.t., which makes it difficult to determine the diurnal variations. Based on the data available, there does not seem to be much payoff for preparing separate tables for different times of day and different seasons for the geographic areas that might be represented by the five stations.

There does appear to be a significant difference between the correlates of stations E, N, and C, North latitudes 35°, 50°, and 52° 45', respectively. The ballistic density at 30,000 ft, corresponding to the same surface density, is about one-half percent higher at the lower latitude stations than at station C. The surface densities run higher at station C. The upper air density may decrease more rapidly than it does at the other stations, resulting in lower ballistic densities for the same surface density.

Data by season do not appear to correlate differently, except at station C. The largest difference noted here was for surface density 1.03, where the ballistic density at 30,000 ft was about one percent lower in summer than in other seasons.

While the procedure presented in this report has been used on only five stations that have an oceanic climate, it should be possible to use essentially the same procedure for processing data from stations where the climate is more affected by land masses. Some modifications might be required, since the temperature lapse rate might be quite different. The diurnal and seasonal variations in pressure and temperature are normally much larger over land masses than they are over large bodies of water.

A similar but earlier study² was made by the Army Electronics Command, Fort Monmouth, New Jersey. Data from land-based stations were used in this study and a number of tables were prepared for each geographic area, season, and time of day.

CONCLUSIONS

1. There does appear to be a good correlation between the surface density and the density at various altitudes over the mid-ocean areas studied.
2. The resulting correlations are different for different latitudes. They do not change appreciably with diurnal time or season over the areas studied.
3. The differences between surface and upper atmospheric conditions are much larger over littoral areas.
4. The procedure described in this report for determining the correlation between upper air density and the surface density may be used for a variety of stations with only minor modifications to the procedure.
5. While the procedure for estimating ballistic density was developed primarily for firing Navy guns, it may also be useful to predict the ballistic density for air-launched missiles.
6. It is estimated that the density ratios at altitudes not to exceed 36,000 ft may be predicted with an error not to exceed 1.0 percent, using the correlation between the surface density and the density of the upper atmosphere.
7. It is estimated that the ballistic density may be predicted with an error not to exceed 0.5 percent in 90 percent of the cases where the altitude does not exceed 36,000 ft.
8. It is estimated that the ballistic density may be predicted with an error between one and two percent where the altitude is between 36,000 and 50,000 ft. This error could be reduced somewhat if the data used in the study had been collected with present day equipment.

RECOMMENDATIONS

1. Correlations should be obtained for other latitudes, including both maritime and beach areas of strategic importance.
2. More data should be obtained for the extremely low and high surface densities.
3. A further study should be conducted to determine how the procedure of estimating the ballistic density, as described in this report, could be implemented in fire control systems and in preparation of range tables.
4. Consideration should be given to using the analytic expression for density in computer programs that simulate the trajectories of unguided missiles.

TR 82-81

REFERENCES

1. U.S. Naval Academy, *Range and Ballistic Tables*, 1935, p. 84.
2. Marvin J. Lowenthal, *The Accuracy of Ballistic Density Departure Tables 1934-1972*, ECOM-5436, OSD 1366 (April 1972).
3. Committee on Extension to the Standard Atmosphere, *U.S. Standard Atmosphere, 1976*, (Washington, D.C.: Government Printing Office, 1976).

TR 82-81

APPENDIX A
A NONLINEAR LEAST-SQUARES TECHNIQUE

A NONLINEAR LEAST-SQUARES TECHNIQUE

Statement of the Problem

Let (x_i, y_i) , $i = 1, 2, \dots, N$ be a set of N data points and

$$f(x, a_1, a_2, \dots, a_M) \quad (A-1)$$

be a function with x as the independent variable. (a_j) , $j = 1, 2, \dots, M$ are parameters of the function and the function may not be linear in these parameters.

We would like to determine values of the M parameters such that

$$F(a_1, a_2, \dots, a_M) = \sum_{i=1}^{i=N} w_i [y_i - f(x_i, a_1, a_2, \dots, a_M)]^2 \quad (A-2)$$

is a minimum. This is the least-squares solution, which is the same as minimizing the sum of the squares of the residuals. A weight w_i is assigned to each data point.

For simplicity of notation, we let

$$f_i(a) = f(x_i, a_1, a_2, \dots, a_M), i = 1, 2, \dots, N \quad (A-3)$$

where $a = (a_1, a_2, \dots, a_M)$. The only restriction on the function $f_i(a)$ is that the partial derivatives of the function with respect to the M parameters be continuous in all of the arguments.

This implies that $f_i(a)$ is a function that can be differentiated.

We assume that these partial derivatives exist at a point \bar{a} , and in some neighborhood about \bar{a} , which includes the point a . Let

$$a = \bar{a} + \Delta a \quad (A-4)$$

TR 82-81

where $\bar{a} = (\bar{a}_1, \bar{a}_2, \dots, \bar{a}_M)$ and $\Delta a = (\Delta a_1, \Delta a_2, \dots, \Delta a_M)$.

If $f_i(a)$ can be differentiated at \bar{a} , then the differential at \bar{a} is an approximation to $f_i(a) - f_i(\bar{a})$ and $f_i(a) - f_i(\bar{a}) = O(\Delta a)(a \rightarrow \bar{a})$.

Thus,

$$f_i(a) - f_i(\bar{a}) = \sum_{j=1}^{j=M} \frac{\partial f_i(\bar{a})}{\partial a_j} \Delta a_j + E(\Delta a) \quad (A-5)$$

where $E(\Delta a) \rightarrow 0$ as $\Delta a \rightarrow 0$ for $i = 1, 2, \dots, N$.

If the approximation \bar{a} is close enough to the solution a , then the problem is considered solved when

$$|a_j - \bar{a}_j| = |\Delta a_j| \leq T, \quad j = 1, 2, \dots, M \quad (A-6)$$

where T = desired precision for the solution.

Formulation of Solution

We now derive the formulation for finding Δa . The solution a is then equal to $\bar{a} + \Delta a$.

Using equation (A-5), we form the overdetermined system of equations ($N > M$)

$$y_i = f_i(a) = f_i(\bar{a}) + \sum_{j=1}^{j=M} \frac{\partial f_i(\bar{a})}{\partial a_j} \Delta a_j \quad (A-7)$$

for data points $i = 1, 2, \dots, N$.

The system of equations used to find Δa becomes

$$\frac{\partial f_i(\bar{a})}{\partial a_1} \Delta a_1 + \frac{\partial f_i(\bar{a})}{\partial a_2} \Delta a_2 + \dots + \frac{\partial f_i(\bar{a})}{\partial a_M} \Delta a_M = Y_i - f_i(\bar{a}) \quad (A-8)$$

($i = 1, 2, \dots, N$).

The system of observational equations (A-8) can now be written in matrix form as given by

$$AX = Y \quad (A-9)$$

where,

$$A = \begin{bmatrix} \frac{\partial f_1(\bar{a})}{\partial a_1} & \frac{\partial f_1(\bar{a})}{\partial a_2} & \dots & \frac{\partial f_1(\bar{a})}{\partial a_M} \\ \frac{\partial f_2(\bar{a})}{\partial a_1} & \frac{\partial f_2(\bar{a})}{\partial a_2} & \dots & \frac{\partial f_2(\bar{a})}{\partial a_M} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial f_N(\bar{a})}{\partial a_1} & \frac{\partial f_N(\bar{a})}{\partial a_2} & \dots & \frac{\partial f_N(\bar{a})}{\partial a_M} \end{bmatrix}$$

$$X = \begin{bmatrix} \Delta a_1 \\ \Delta a_2 \\ \vdots \\ \vdots \\ \Delta a_M \end{bmatrix}$$

TR 82-81

$$Y = \begin{pmatrix} y_1 - f_1(\bar{a}) \\ y_2 - f_2(\bar{a}) \\ \vdots \\ \vdots \\ y_N - f_N(\bar{a}) \end{pmatrix}$$

The column matrix Y is called the residual matrix. Solving matrix equation (A-9) yields the normal equations in matrix form

$$A^T A X = A^T Y \quad (A-10)$$

If the residuals are to be weighted, we can include the weight matrix W where,

$$W = \begin{pmatrix} w_1 & & & \\ & w_2 & 0 & \\ 0 & & \ddots & \\ & & \ddots & \\ & & & w_N \end{pmatrix}, \quad (A-11)$$

Completing the solution to the matrix equation (A-10) and upon including the weight matrix, we have

$$X = (A^T W A)^{-1} A^T W Y \quad (A-12)$$

X is the least-squares solution to the system of equations (A-8) with the weights included. Elements of the X matrix are now tested in absolute value against the tolerance T. If the tolerance test is satisfied, we are done and the least-square solution to equation (A-2) is given by

$$a_j = \bar{a}_j + \Delta a_j, \quad j = 1, 2, \dots, M \quad (A-13)$$

TR 82-81

Whenever the tolerance test fails, equation (A-13) gives the next approximation and the iteration process is repeated with matrix equation (A-12) until the tolerance test is satisfied.

Remarks

Once an acceptable solution has been found, it may be desirable to know how well the function fits the given data. Analysis for how well the solution fits can usually be made by examining the residuals for each observation.

The variances for the solution (a) can be found from the variance, covariance matrix.

If the variances and residuals are large, a different approximating function $f_i(a)$ may be tested.

When polynomials are used for testing, the residuals will drop off rapidly as the degree of the polynomial increases from one. Further increase in the degree of the polynomial will show little improvement of the residuals.

TR 82-81

APPENDIX B

AN ALTERNATE METHOD FOR COMPUTING DENSITY

AN ALTERNATE METHOD FOR COMPUTING DENSITY

Since the procedure used to fit the observed densities provided little information as to why the correction term for altitudes below 3,500 ft improved the fit, an investigation was made using a sample set of data obtained from 25 sondes. The sondes were taken consecutively from the group that had been sorted according to season after the surface densities were arranged in numerical order. The median of the surface densities in the sample was equal to the U.S. Standard density at mean sea level. The sondes were released at station E during the spring season, 1200 hr G.m.t.

Separate least-squares fits were made to the pressure and temperature in the altitude range from 0 to 36,089 ft. No attempt was made to fit the temperature or pressure above 36,089-ft altitude.

The equation used to fit the pressure is similar to equation (1)

$$P = p_1 e^{(p_2 h)} + p_3 h \quad (B-1)$$

where

P is the pressure (mb)

h is the altitude (ft)

p_1 , p_2 , and p_3 are constants determined in the least-squares fit

The observed temperatures were first converted to virtual temperatures with the equation

$$TV = \frac{T}{1.0 - \frac{0.3783 * RH * V}{P}} \quad (B-2)$$

where

TV is the virtual temperature ("K)

T is the observed temperature ("K)

RH is the observed relative humidity (dimensionless)

V is the saturation vapor pressure (mb)

P is the observed pressure (mb)

Several least-squares fits were made with the virtual temperature in the altitude range from 0 to 36,089 ft using polynomials that, in every case, produced large residuals below 5,000 ft. A big improvement was made by segmenting the data into three zones, 0 to 3,500, 3,501 to 6,000, and 6,001 to 36,089 ft. A one-degree polynomial least-squares fit was used in the two lower zones and a third-degree polynomial was used in the upper zone. The intersections of the equations are located at 3,731 and 5,270 ft which were used to define the boundaries of the zones.

The density was computed with the equation

$$\rho = P/(R*T) \quad (B-3)$$

where

ρ is the density (lb/ft^3)

P is the pressure determined by a least-squares fit (mb)

T is the temperature determined by a least-squares fit ($^{\circ}K$)

R is a constant, 45.981610868

Computing the density in this manner made a small reduction in the mean of the residuals but no improvement in the standard deviation. While a single function fits the pressure from sea level to 36,089 ft, the nonlinearity in the temperature profile is quite apparent. The lapse rate in the temperature based on the least-squares fit from sea level to 3,731 ft is $2.60^{\circ}C$ per 1,000 ft and $0.358^{\circ}C$ per 1,000 ft from 3,731 to 5,270 ft using the intersections of the equations to define the zone boundaries. The average lapse rate based on the least-squares fit in the zone from 5,270 to 36,089 ft is $1.99^{\circ}C$ per 1,000 ft. The latter value is in good agreement with the lapse rate of $1.98^{\circ}C$ per 1,000 ft from sea level to 36,089 ft that was used to define the U.S. Standard atmosphere.

Profiles of the temperature and pressure obtained with the least-squares fit are shown in Figures B-1 and B-2, respectively. A profile of the density computed

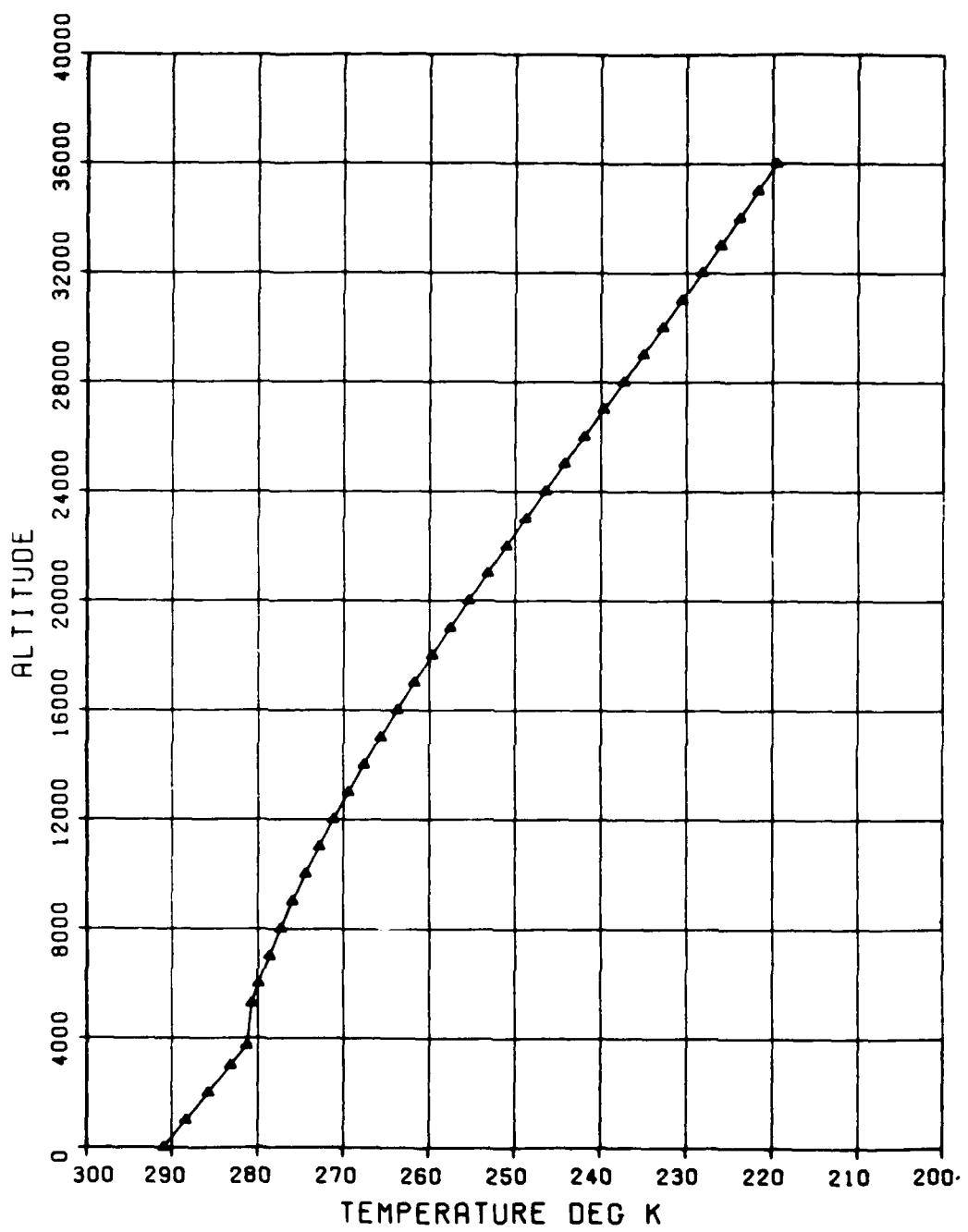


FIGURE B-1. STATION F SPRING 1200 hr G.m.t.
Temperature profile based on three least-squares fits, linear 0 - 3,500, linear
3,500 - 6,000, and third-degree polynomial 6,000 - 3,600 ft. The equations were
spliced at 3,730 and 5,270 ft.

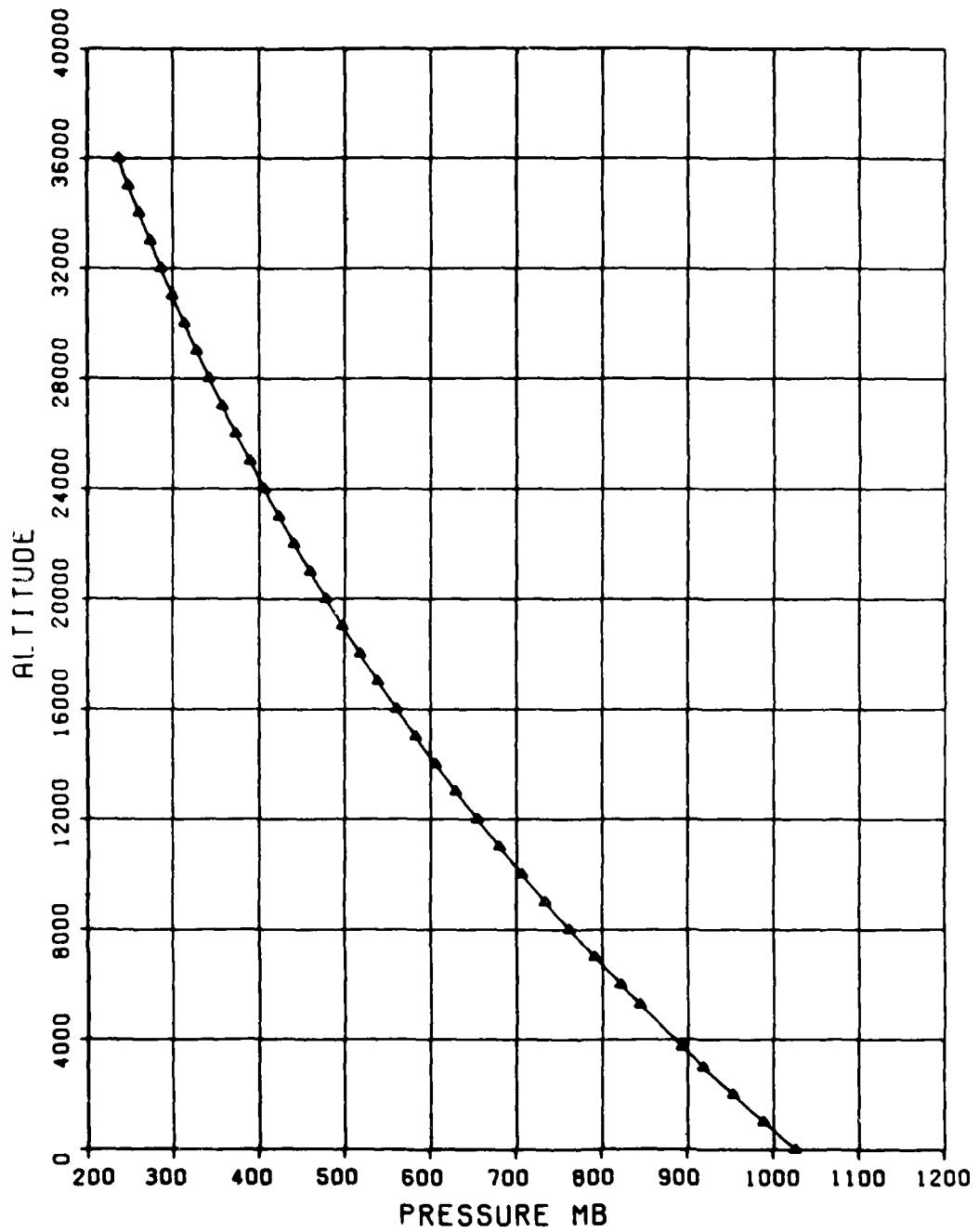


FIGURE B-2. STATION E 1200 hr G.m.t.
Pressure profile based on a least-squares fit with an exponential function.

with equation (7) is shown in Figure B-3. For comparison, Figure B-4 is a profile of the density computed with equations (1) and (3) where the coefficients were obtained by making a least-squares fit to the observed densities. Very little difference can be seen when curves of Figures B-3 and B-4 are superimposed.

From these results—(1) the small difference in the residuals between the two methods of calculating densities, and (2) indiscernible difference in the two curves obtained—it appears that there is no advantage in computing density from smoothed temperature and pressure data versus smoothed density data. It may be noted that the first method requires 11 undetermined constants, the latter only 4.

The method of making separate least-squares fits to the temperature and pressure does provide a much clearer explanation as to why the correction term in equation (3) improved the fit to the density. The reason is the large variations in the lapse rate of the temperature at the lower altitudes.

The equations used to fit the temperature are

Altitude (ft)

$$\begin{aligned} 0 - 3,500 \quad & \text{Temperature} = a_0 + a_1 h \\ 3,500 - 6,000 \quad & \text{Temperature} = a'_0 + a'_1 h \\ 6,000 - 36,000 \quad & \text{Temperature} = a''_0 + a''_1 h + a''_2 h^2 + a''_3 h^3 \end{aligned}$$

where

temperature is the virtual temperature °K

h is the altitude in feet

The altitudes of intersections are 3,731 and 5,270 ft.

TR 82-81

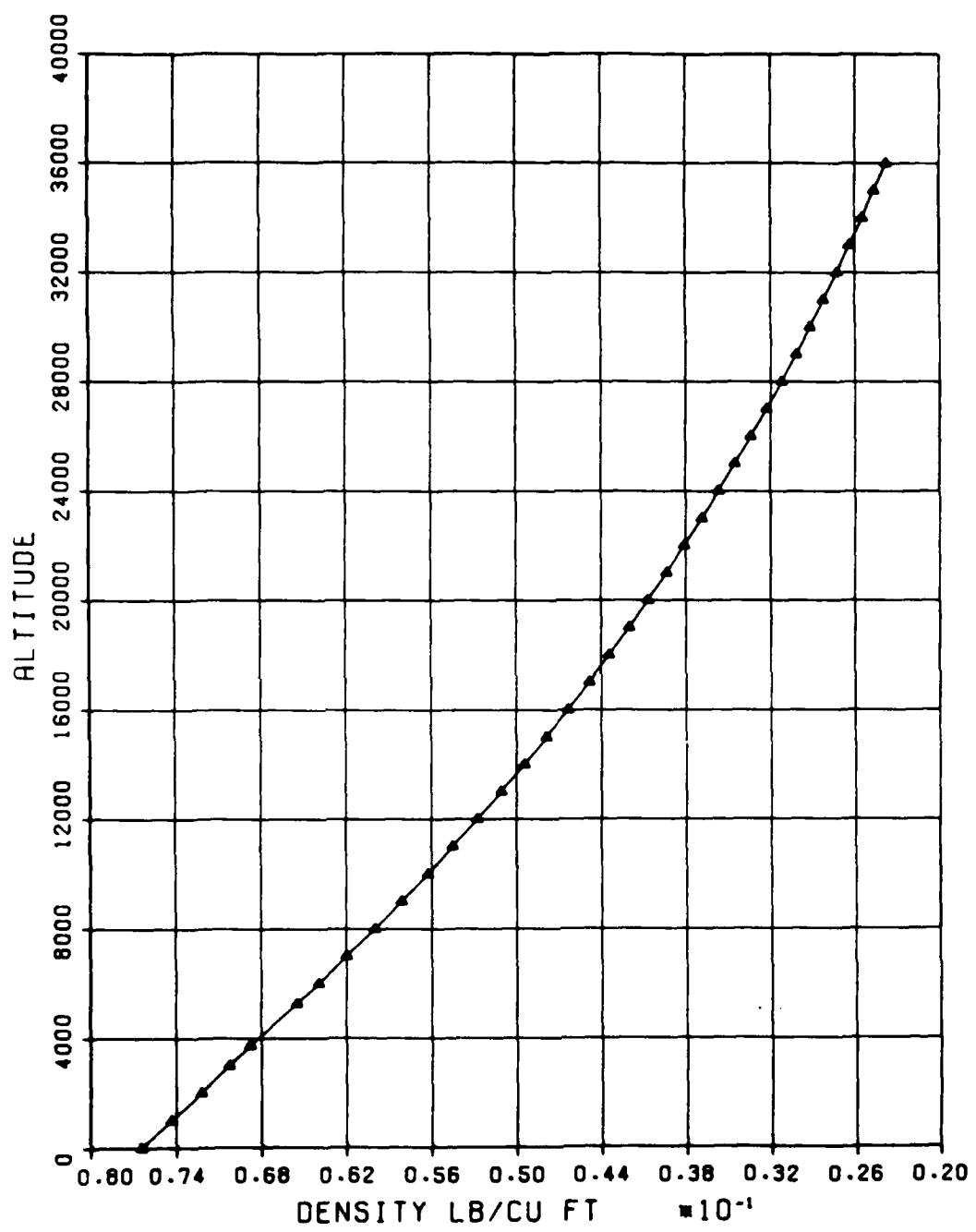


FIGURE B-3.
Density profile computed from the data of Figures B-1 and B-2.

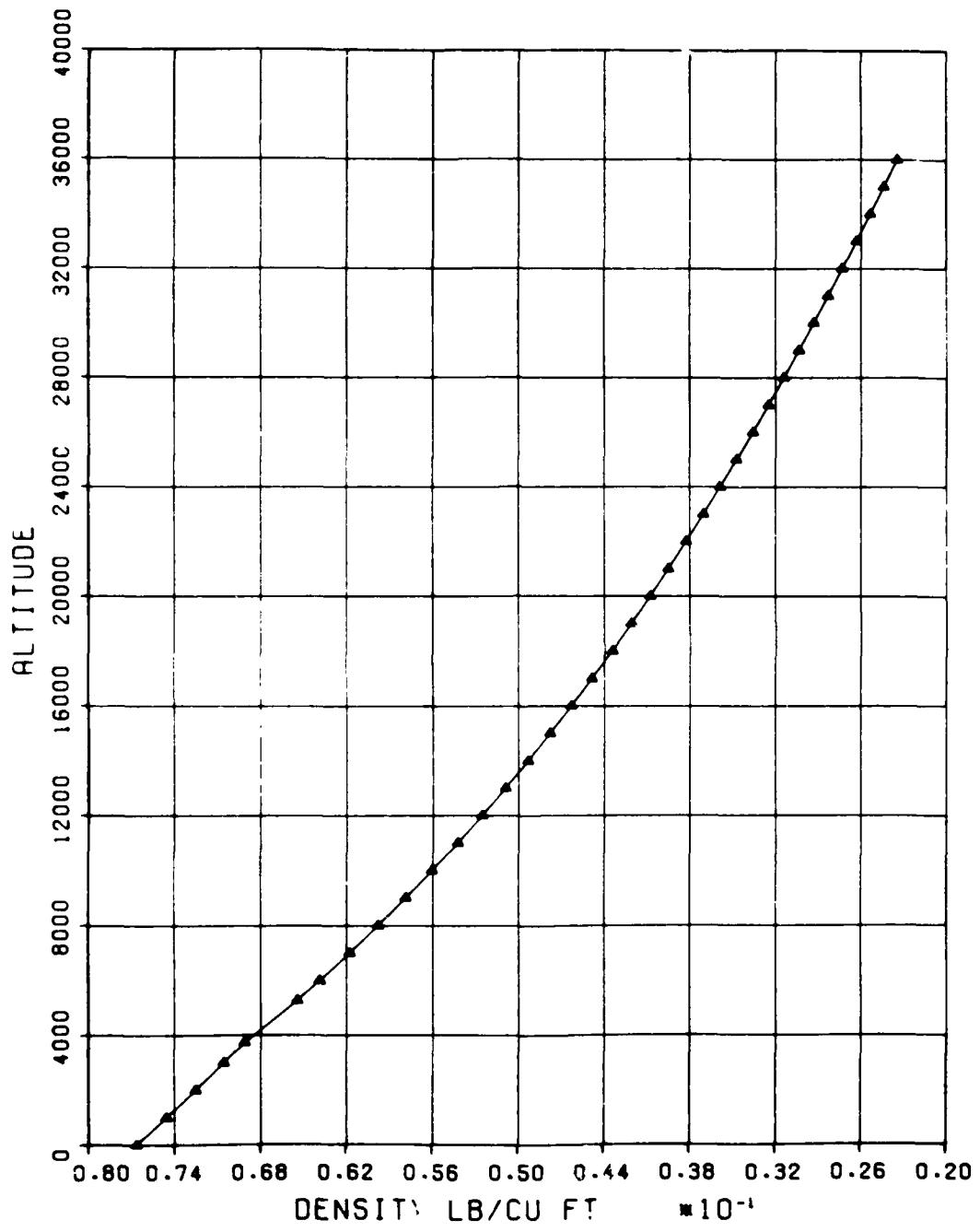


FIGURE B-4. STATION E SPRING 1200 t.r G.m.t.
Density profile computed directly from a least-squares fit to the density.

TR 82-81

The coefficients obtained in the least-squares fit are

$$\begin{aligned}a_0 &= 0.29098019920169 \text{ E+3} \\a_1 &= -0.26010921095663 \text{ E-2} \\a'_0 &= 0.28261034232183 \text{ E+3} \\a'_1 &= -0.35814511053088 \text{ E-3} \\a''_0 &= 0.28474414363984 \text{ E+3} \\a''_1 &= -0.42144325442356 \text{ E-3} \\a''_2 &= -0.69303432938534 \text{ E-7} \\a''_3 &= 0.85246672752231 \text{ E-12}\end{aligned}$$

The mean and standard deviations of the residuals divided by the computed values are

<u>Altitude (ft)</u>	<u>Mean</u>	<u>Sigma</u>	<u>N</u>
0 - 3,500	-0.00000002	0.00603867	98
3,500 - 6,000	0.00000000	0.01019354	76
6,000 - 36,000	-0.00000008	0.01654041	357
0 - 36,000	-0.00000362	0.01433263	531

N is the number of data points in the fit.

The temperature profile is shown in Figure B-1.

The equation used to fit the pressure is

$$P = c_1 * e^{(c_2 h)} + c_3 h$$

where

P is pressure in mb

h is the altitude in feet

The coefficients obtained in the least-squares fit are

$$\begin{aligned}c_1 &= 0.1025894426895 \text{ E+4} \\c_2 &= -0.3512226501974 \text{ E-4} \\c_3 &= -0.1469124958633 \text{ E-2}\end{aligned}$$

The mean and standard deviation of the residuals divided by the computed values are

<u>Altitude (ft)</u>	<u>Mean</u>	<u>Sigma</u>	<u>N</u>
0 - 36,000	-0.00000270	0.01171363	531

N is the number of data points in the fit.

The pressure profile is shown in Figure B-2.

The density profile shown in Figure B-3 was computed with the equation

$$\rho = P/(R*T)$$

where

ρ is the density (lb/ft^3)

P is the pressure (mb)

T is the virtual temperature ($^{\circ}\text{K}$)

R is a constant, 45.981610868

The mean and standard deviation of the residuals divided by the computed value are

<u>Altitude (ft)</u>	<u>Mean</u>	<u>Sigma</u>	<u>N</u>
0 - 36,000	0.00009937	0.01129087	531

The density profile shown in Figure B-4 for altitudes below 3,500 ft was computed with the equation,

TR 82-81

$$\rho = c_1 e^{(c_2 h)} + c_3 h + (\rho_0 - c_1) \left| \frac{3500 - h}{3500} \right|$$

and for altitudes equal to or greater than 3,500 ft was computed with the equation

$$\rho = c_1 e^{(c_2 h)} + c_3 h$$

which is the same procedure described previously in the report. The coefficients used to create the profile are

$$\begin{aligned}c_1 &= 0.076640263730 \text{ (lb/ft}^3\text{)} \\c_2 &= -0.304780287061 \text{ E-4 (ft}^{-1}\text{)} \\c_0 &= 0.076474 \text{ (lb/ft}^3\text{)} \\c_3 &= -0.517405589378 \text{ E-7 (lb/ft}^4\text{)}\end{aligned}$$

The mean and standard deviation of the residuals divided by the computed value are

<u>Altitude (ft)</u>	<u>Mean</u>	<u>Sigma</u>
0 - 36,000	0.00048651	0.01160715

TR 82-81

APPENDIX C

COEFFICIENTS OBTAINED BY FITTING OBSERVED DENSITY

In this appendix, four lines of data appear for each group of sondes that were used in the least-squares fit.

Lines 1 and 2:

<u>Item</u>	<u>Identification</u>	<u>Description</u>
1	N	Number of data points that met tolerances
2	JE	Number of points used in fit
3	AMEAN	Mean of the residuals
4	SIGMA	Standard deviation of the residuals

Line 1 is for the altitude range from 0 to 36,089 ft, and Line 2 is for the altitude range 36,089 to 65,000 ft. The first five items in Lines 3 and 4 are coefficients C_1 , C_2 , and C_3 for equation (1), which were obtained by making a least-squares fit in the altitude range 3,500 to 36,089 ft, and coefficients C_4 and C_5 for equation (2), which were obtained by making a least-squares fit in the altitude range 36,089 to 65,000. The coefficients are listed in the order of their subscripts. The next item on Line 4 is the median of the surface densities of the sondes used in the fit. The last item is a counter and has no significance.

Data points refer to the individual altitudes where temperature, pressure, and humidity were recorded. The residuals were expressed as a ratio of the residual to the density obtained with the least-squares fit as stated previously. No data points were eliminated in the least-squares fit; but tolerances on the residuals were specified, and the number of points that met the tolerances were recorded. The tolerance used in the lower altitude region was 0.025, and in the higher region it was 0.150. A few tests were made to eliminate bad data points before the least-squares fit was performed.

STATION E 00HR FOUR SEASONS

WINTER

106 N	106 JE	.00009371	AMEAN	.00499973 SIGMA
37 N	37 JE	.00053558	AMEAN	.01342884 SIGMA
*075079281683	-.294862954960E-04	-.697033163821E-07	-450764290603E-04	
-0.159550178886E-07	.07418000	1		
535 N	547 JE	.00004310	AMEAN	.01235709 SIGMA
173 N	176 JE	-.00032082	AMEAN	.03395270 SIGMA
*075746131856	-.305628508314E-04	-.518345657782E-07	-409038381380E-04	
-0.449743040887E-07	.07494500	2		
547 N	553 JE	.00006191	AMEAN	.00879245 SIGMA
198 N	198 JE	-.00192602	AMEAN	.02936409 SIGMA
*076519989588	-.301148012167E-04	-.627915978676E-07	-451529783579E-04	
-0.147871540870E-07	.07570900	3		
585 N	592 JE	.00021436	AMEAN	.00852413 SIGMA
230 N	230 JE	-.00062556	AMEAN	.03150237 SIGMA
*077508432763	-.305740514838E-04	-.500335521527E-07	-457665151713E-04	
-0.980870348999E-08	.07647400	4		
624 N	632 JE	.00033378	AMEAN	.00946879 SIGMA
240 N	240 JE	-.0009101	AMEAN	.03334458 SIGMA
*078881310762	-.323681211507E-04	-.199368741673E-07	-459876070910E-04	
-0.162405407298E-07	.07723900	5		
106 N	107 JE	.00001313	AMEAN	.00984285 SIGMA
46 N	46 JE	-.00164000	AMEAN	.02560609 SIGMA
*080252489385	-.3388561615734E-04	-.560937162076E-08	-507730626667E-04	
-0.150172841422E-07	.07800300	6		

SPRING

85 N	85 JE	-.00012323	AMEAN	.00419959 SIGMA
33 N	33 JE	-.00032452	AMEAN	.03489420 SIGMA
*074353805262	-.284235206192E-04	-.941032720434E-07	-380570178375E-04	
-0.727382338584E-07	.07418000	7		
716 N	721 JE	.00013955	AMEAN	.00629754 SIGMA
271 N	271 JE	-.00106141	AMEAN	.03009369 SIGMA
*075733087556	-.300418665094E-04	-.551187072110E-07	-394703344566E-04	

- .625403819063E-07	.07494500	8	
594 N	605 JE	* 00023908 AMEAN	* 01023382 SIGMA
220 N	220 JE	* 00131510 AMEAN	* 02999632 SIGMA
* 076742754647	- .306830920088E-04	- .505840324145E-07	- .421123394770E-04
- .42310572703E-07	.07570900	9	
529 N	535 JE	* 00046346 AMEAN	* 00960208 SIGMA
205 N	205 JE	- .0008578 AMEAN	* 03557140 SIGMA
* 077239352033	- .312365997541E-04	- .342772620491E-07	- .428263016612E-04
- .368989089084E-07	.07647400	10	
115 N	117 JE	* 00084830 AMEAN	* 01277639 SIGMA
44 N	44 JE	* 00242485 AMEAN	* 02579073 SIGMA
* 076432436906	- .319666630560E-04	- .245952632508E-07	- .465006812171E-04
- .126913193672E-07	.07723900	11	
SUMMER			
39 N	39 JE	* 00003057 AMEAN	* 00442968 SIGMA
13 N	13 JE	* 00188364 AMEAN	* 01798935 SIGMA
* 074002617454	- .299262474105E-04	- .455109721199E-07	- .306666378990E-04
- .135069282391E-06	.07265000	12	
557 N	557 JE	* 00005280 AMEAN	* 00495224 SIGMA
172 N	172 JE	* 00196325 AMEAN	* 01876588 SIGMA
* 074411095244	- .294635397582E-04	- .579634937653E-07	- .329739352781E-04
- .114864418235E-06	.07341500	13	
582 N	583 JE	* 00025465 AMEAN	* 00554850 SIGMA
167 N	167 JE	* 00180320 AMEAN	* 02114770 SIGMA
* 075116341423	- .293381346612E-04	- .643063602866E-07	- .346008755020E-04
- .100301112936E-06	.07418000	14	
601 N	601 JE	* 00008318 AMEAN	* 00651381 SIGMA
167 N	167 JE	* 00170740 AMEAN	* 02126472 SIGMA
* 076057514114	- .302017801903E-04	- .508650826689E-07	- .356795725945E-04
- .666673039486E-07	.07494500	15	
65 N	66 JE	* 00044599 AMEAN	* 00916910 SIGMA
33 N	33 JE	* 00145388 AMEAN	* 02100466 SIGMA
* 07650364671	- .324380267945E-04	* 251304420554E-08	- .344656943297E-04
- .103369959675E-06	.07570900	16	

FALL		76 N	76 JE	• 000 32131 AMEAN	• 00639478 SIGMA
30 N		30 JE	• 000 66376 AMEAN	• 03100741 SIGMA	
• 074885189662	-07375737339E-07	-0.297345986104E-04	-0.570098172919E-07	-0.368081504810E-04	
552 N	557	JE	• 000 31220 AMEAN	• 00706654 SIGMA	
185 N	185	JE	• 000 01647 AMEAN	• 03334804 SIGMA	
• 075059277710	-0.296044770631E-04	-0.623120720704E-07	-0.366529441989E-04		
• 0818355014763E-07	.07419000	18			
566 N	568	JE	• 000 16250 AMEAN	• 00716179 SIGMA	
219 N	219	JE	• 000 47250 AMEAN	• 03144311 SIGMA	
• 075989481796	-0.306654221840E-04	-0.394741248165E-07	-0.396086519246E-04		
• 0606548996052E-07	.07494500	19			
579 N	584	JE	• 060 20431 AMEAN	• 00897739 SIGMA	
231 N	231	JE	• 080 60221 AMEAN	• 02636899 SIGMA	
• 077258445293	-0.315266459161E-04	-0.259998924279E-07	-0.440922708535E-04		
• 0.260602884661E-07	.07570900	20			
124 N	124	JE	• 000 023166 AMEAN	• 00855050 SIGMA	
41 N	41	JE	• 002 15124 AMEAN	• 02388429 SIGMA	
• 078307086422	-0.317086362801E-04	-0.337162153010E-07	-0.486503319257E-04		
• 169464336075E-06	.07647400	21			
STATION E 00HR GMT SEASONS COMBINED					
55 N	55	JE	-0.000 13503 AMEAN	• 00438076 SIGMA	
21 N	21	JE	• 001 53047 AMEAN	• 01751126 SIGMA	
• 073916454338	-0.2971683716810E-04	-0.5264466694805E-07	-0.288613372848E-04		
• 0.153449666026E-06	.07265000	1			
542 N	543	JE	• 000 007340 AMEAN	• 00521675 SIGMA	
168 N	168	JE	• 001 02577 AMEAN	• 02135036 SIGMA	
• 0.074461986973	-0.294345939465E-04	-0.506052812264E-07	-0.341636027919E-04		
• 103945419144E-06	.07344500	2			
561 N	561	JE	• 000 34351 AMEAN	• 00611733 SIGMA	
174 N	174	JE	• 007 8476 AMEAN	• 02222567 SIGMA	
• 075164029585	-0.296631277419E-04	-0.573271511476E-07	-0.366071002444E-04		
• 798583050256E-07	.07418000	3			
629 N	633	JE	• 000 06990 AMEAN	• 00743407 SIGMA	

236 N 239 JE .00077494 AMEAN .03043555 SIGMA
 * 076003913198 -.305940735172E-04 -.416309714657E-07 -.404390269412E-04
 -.50 6645843921E-07 .07494500 4
 539 N 550 JE .00024759 AMEAN .01056239 SIGMA
 161 N 101 JE .00111095 AMEAN .02725811 SIGMA
 * 076678434996 -.308753218587E-04 -.446318169070E-07 -.421188254661E-04
 -.406749569099E-07 .07570900 5
 585 N 592 JE .00015789 AMEAN .00039561 SIGMA
 226 N 226 JE -.00095049 AMEAN .03406700 SIGMA
 * 077586192104 -.311540064632E-04 -.422547625365E-07 -.450706163171E-04
 -.180519540787E-07 .07647400 6
 548 N 555 JE .00046953 AMEAN .01040682 SIGMA
 225 N 225 JE .00093193 AMEAN .03213343 SIGMA
 * 078649231085 -.323476217940E-04 -.168946267275E-07 -.457746168953E-04
 -.188835761990E-07 .07723900 7
 155 N 157 JE .00015486 AMEAN .01001072 SIGMA
 70 N 70 JE -.00117266 AMEAN .02554801 SIGMA
 * 080008865235 -.332939606239E-04 -.482455101442E-08 -.507021981509E-04
 *.138064671447E-07 .07800300 8
 31 N 40 JE -.00142227 AMEAN .02145617 SIGMA
 16 N 16 JE .00136873 AMEAN .01108424 SIGMA
 * 080111099019 -.346798589829E-04 .402026625526E-07 -.4905768763369E-04
 -.57 0790632045E-08 .07876800 9

STATION E 12HR FOUR SEASONS

WINTER
 155 N 155 JE -.00008078 AMEAN .000489720 SIGMA
 37 N 37 JE .00023310 AMEAN .02602642 SIGMA
 * 075030877430 -.309326914880E-04 -.550372354609E-07 -.395274000044E-04
 -.543206237525E-07 .07418000 1
 545 N 557 JE -.00010871 AMEAN .01084876 SIGMA
 216 N 216 JE -.00065341 AMEAN .03205415 SIGMA
 * 076197196680 -.303223535410E-04 -.601704522812E-07 -.459187309579E-04
 -.588017794425E-08 .07494500 2

591 N	594 JE	* 00011055	AMEAN	* 00709901 SIGMA
249 N	245 JE	- 00065312	AMEAN	* 02425463 SIGMA
* 077022282557	- .310423451067E-04	- .426056661647E-07	- .461343999269E-04	
- .795500050002E-06	.07570900	3		
335 N	335 JE	* 00026528	AMEAN	* 00999205 SIGMA
146 N	146 JE	* 00002409	AMEAN	* 02270905 SIGMA
* 077020361702	- .314542580480E-04	- .3472220880006E-07	- .432410190256E-04	
- .332274942909E-07	.07647400	4		
611 N	617 JE	* 00029613	AMEAN	* 00906797 SIGMA
254 N	254 JE	- * 00133092	AMEAN	* 02051303 SIGMA
* 079150387943	- .330580221397E-04	- .215356284127E-06	- .483625659055E-04	
- .807231527157E-09	.07723900	5		

SPRING

219 N	216 JE	- 00005360	AMEAN	* 00369571 SIGMA
95 N	95 JE	* 00121376	AMEAN	* 03599471 SIGMA
* 075123190148	- .295923492901E-04	- .685606999806E-07	- .415998156953E-04	
- .406396599472E-07	.07418000	5		
572 N	576 JE	* 00011338	AMEAN	* 00738243 SIGMA
240 N	240 JE	* 00003964	AMEAN	* 03431977 SIGMA
* 075830354575	- .302078603356E-04	- .543715278413E-07	- .402946907470E-04	
- .534643663213E-07	.07494500	7		
524 N	528 JE	* 00039618	AMEAN	* 01730689 SIGMA
214 N	214 JE	* 00163039	AMEAN	* 02414344 SIGMA
* 0766640263730	- .30473028761E-04	- .517405589378E-07	- .410525537453E-04	
- .484707804362E-07	.07570900	8		
522 N	531 JE	* 00048651	AMEAN	* 01160715 SIGMA
253 N	255 JE	* 00024623	AMEAN	* 02951284 SIGMA
* 077487922568	- .313676919544E-04	- .353021223364E-07	- .438039057253E-04	
- .292856394714E-07	.07647400	9		
101 N	102 JE	* 00157044	AMEAN	* 01217757 SIGMA
27 N	27 JE	* 00001065	AMEAN	* 01501577 SIGMA
* 078733576672	- .330111444160E-04	* 166763630665E-06	- .474730682042E-04	
- .844893833634E-08	.07723900	10		

SUMMER

562 N	562 JE	.00003631	AMEAN	.00576280	SIGMA
242 N	242 JE	.00167801	AMEAN	.02170284	SIGMA
* 074541372461	- 296703645956E-04	- .554732911082E-07	- .335399439230E-04		
- 109059773373E-06	.07341500	11			
532 N	532 JE	.00029180	AMEAN	.00516922	SIGMA
171 N	171 JE	.00100929	AMEAN	.01445597	SIGMA
* 075214489043	- 294920244574E-04	- .616491043396E-07	- .36167762944E-04		
- 840571249790 E-07	.07418000	12			
504 N	507 JE	.00030070	AMEAN	.02256684	SIGMA
196 N	196 JE	.00189725	AMEAN	.02122023	SIGMA
* 075858349635	- 299037346719E-04	- .568828999155E-07	- .353067485094E-04		
- 940225706960 E-07	.07494500	13			
 FALL					
101 N	103 JE	.00036658	AMEAN	.01249749	SIGMA
28 N	26 JE	.00178426	AMEAN	.01635500	SIGMA
* 075306975714	- 316199839816E-04	- 126806169220E-07	- 382494516627E-04		
- 716522639671 E-07	.07341500	14			
584 N	585 JE	.00024980	AMEAN	.00557367	SIGMA
257 N	257 JE	.00105104	AMEAN	.02811453	SIGMA
* 075244152320	- 304716383621E-04	- 39009796857E-07	- 364552200297E-04		
- 862710989754 E-07	.07418000	15			
500 N	503 JE	.00028466	AMEAN	.00855190	SIGMA
198 N	198 JE	.00073576	AMEAN	.02917977	SIGMA
* 075879139253	- 306557368546E-04	- 391173189122E-07	- 3777102865554E-04		
- 7440683886949E-07	.07494500	16			
537 N	541 JE	.00035236	AMEAN	.01068197	SIGMA
225 N	225 JE	- .00026563	AMEAN	.02507366	SIGMA
* 077099881194	- .309308827165E-04	- .463637399804E-07	- .407976746180E-04		
- 502856873135E-07	.07570900	17			
189 N	192 JE	- .00001691	AMEAN	.01039020	SIGMA
81 N	81 JE	.00041722	AMEAN	.03495259	SIGMA
* 078636487486	- .333417573130E-04	* 306983969321E-08	- .434169559436E-04		
- 392624149192 E-07	.07647400	18			

83 N 83 JE - .00021132 AMEAN .00586070 SIGMA
 40 N 40 JE .00209744 AMEAN .02342494 SIGMA
 *074046534670 -.297621698012E-04 -.561603633550E-07 -.304381710796E-04
 -*132484417091E-06 .07265000 1
 564 N 566 JE .00007565 AMEAN .00749577 SIGMA
 229 N 225 JE .00177311 AMEAN .02145995 SIGMA
 *074764931991 -.300376322102E-04 -.475062967547E-07 -.360757002530E-04
 -*104346667678E-06 .07341500 2
 559 N 559 JE .00019089 AMEAN .00628409 SIGMA
 226 N 227 JE .00093570 AMEAN .03109516 SIGMA
 *075164001806 -.297553589230E-04 -.575532631951E-07 -.3786555930475E-04
 -*718505014332E-07 .07419000 3
 546 N 548 JE .00026285 AMEAN .00781521 SIGMA
 175 N 175 JE -.00023137 AMEAN .03879552 SIGMA
 *075999033383 -.305589095068E-04 -.459294593779E-07 -.389371012515E-04
 -*64044013895E-07 .07494500 4
 549 N 553 JE .00033323 AMEAN .00928353 SIGMA
 229 N 225 JE .00091876 AMEAN .02443316 SIGMA
 *.076847976664 -.308670522879E-04 -.4460103227586E-07 -.423018423799E-04
 -*389831276971E-07 .07570900 5
 539 N 549 JE .00057035 AMEAN .01217471 SIGMA
 256 N 258 JE .00015215 AMEAN .03158384 SIGMA
 *077741410559 -.314122542703E-04 -.3864551540687E-07 -.425026724634E-04
 -*384231641904E-07 .075647400 6
 266 N 268 JE .00014534 AMEAN .00842401 SIGMA
 97 N 97 JE -.00210771 AMEAN .02880930 SIGMA
 *.079161559258 -.332958045749E-04 -.372624763272E-09 -.409510104223E-04
 *.688395383325E-08 .07723900 7
 123 N 124 JE -.00022082 AMEAN .00996760 SIGMA
 75 N 75 JE .00243365 AMEAN .02582058 SIGMA
 *.080305994829 -.346243599295E-04 .248231111476E-07 -.513015102647E-04
 *178521124110E-07 .07800300 8

STATION V 00HR FOUR SEASONS

WINTER						
83 N	83	JE	.00003488	AMEAN	.00067984	SIGMA
27 N	27	JE	-.00009238	AMEAN	.01495347	SIGMA
*074525310138	-.294218657930E-04		-.889947170139E-07		-.357431352087E-04	
-0.759650134623E-07	.07416000	1				
429 N	468	JE	.00021326	AMEAN	.01663872	SIGMA
165 N	165	JE	-.00054370	AMEAN	.02743251	SIGMA
*075840253696	-.287994758650E-04		-.126614671712E-06		-.377219365718E-04	
-0.589023875055E-07	.07494500	2				
521 N	579	JE	.00017659	AMEAN	.01462575	SIGMA
223 N	223	JE	.00067728	AMEAN	.03009421	SIGMA
*076734353922	-.300731732332E-04		-.882602213997E-07		-.401466385334E-04	
-0.475480063265E-07	.07570900	3				
485 N	537	JE	.00021426	AMEAN	.01723880	SIGMA
173 N	173	JE	-.00154323	AMEAN	.02963285	SIGMA
*077994143861	-.302072669337E-04		-.108472239971E-06		-.375602452599E-04	
-0.615770739966E-07	.07647400	4				
484 N	547	JE	.00016713	AMEAN	.01588830	SIGMA
179 N	179	JE	-.00004863	AMEAN	.03214428	SIGMA
*079468035421	-.319857227511E-04		-.684759761459E-07		-.432629505650E-04	
-0.263435881045E-07	.07723900	5				
121 N	128	JE	.00000446	AMEAN	.01377598	SIGMA
39 N	35	JE	.00010086	AMEAN	.02600136	SIGMA
*080502548356	-.326935671221E-04		-.623200361131E-07		-.438780590950E-04	
-0.2332985177E-07	.07800300	6				
SPRING						
331 N	331	JE	-.00021690	AMEAN	.00665090	SIGMA
135 N	135	JE	.00179898	AMEAN	.02282032	SIGMA
*074453385033	-.305400405068E-04		-.389115214540E-07		-.293581924203E-04	
-0.145083536797E-06	.07416000	7				
554 N	554	JE	.00022910	AMEAN	.00674795	SIGMA
224 N	224	JE	.00089275	AMEAN	.02677927	SIGMA
*075297620599	-.307737336106E-04		-.381636865587E-07		-.342898622142E-04	

- . 992698633533E-07	499	JE	* 00069663	AMEAN	* 00 841648 SIGMA
496 N	499	JE	* 00069663	AMEAN	* 02706867 SIGMA
233 N	233	JE	* 00117567	AMEAN	- * 365229419267E-04
* 076375355053	- . 319260819310E-04		- * 151112503285E-07		
- . 026885916713E-07	. 07570900		9		
486 N	491	JE	* 00079095	AMEAN	* 01025155 SIGMA
183 N	183	JE	* 00025417	AMEAN	* 02994907 SIGMA
* 077403076367	- . 319212861014E-04		- * 265096729784E-07		- * 420671940430E-04
- . 38237037019E-07	. 07647400		10		
450 N	479	JE	* 00069546	AMEAN	* 01556209 SIGMA
218 N	218	JE	- * 00075293	AMEAN	* 03164796 SIGMA
* 078506446170	- . 329034979386E-04		- * 121449057635E-07		- * 426025201965E-04
- . 344639618665E-07	. 07723900		11		
77 N	80	JE	* 00111974	AMEAN	* 01556016 SIGMA
32 N	32	JE	- * 00045779	AMEAN	* 03555065 SIGMA
* 080158620606	- . 3380559601999E-04		- * 791389394562E-08		- * 437431445873E-04
- . 250120355242E-07	. 07800300		12		
 SUMMER					
257 N	252	JE	* 00049459	AMEAN	* 00518061 SIGMA
130 N	130	JE	* 00046939	AMEAN	* 01562624 SIGMA
* 073834695782	- . 299075280005E-04		- * 469988143453E-07		- * 293497892563E-04
- . 146006104824E-06	. 07265000		13		
537 N	537	JE	* 00041293	AMEAN	* 00536209 SIGMA
246 N	246	JE	* 00111684	AMEAN	* 01991504 SIGMA
* 074398672355	- . 298644556726E-04		- * 509673466174E-07		- * 303159600471E-04
- . 137255272276E-06	. 07341500		14		
474 N	484	JE	* 00011263	AMEAN	* 00864456 SIGMA
204 N	204	JE	* 00108644	AMEAN	* 02436276 SIGMA
* 074653295496	- . 303068679490E-04		- * 423049486960E-07		- * 301955326060E-04
- . 140801919785E-06	. 07418000		15		
223 N	223	JE	* 00050054	AMEAN	* 00726032 SIGMA
81 N	81	JE	* 00155510	AMEAN	* 02114007 SIGMA
* 075490897693	- . 312039232458E-04		- * 287569972084E-07		- * 295621761640E-04
- . 149857332670E-06	. 07494500		16		
79 N	79	JE	* 00110488	AMEAN	* 00704344 SIGMA

28 N 2E JE *00220634 AMEAN *02351338 SIGMA
 *076452825232 -.322150969424E-04 -.105782531427E-07 -*305438953662E-04
 -*143182030283E-06 .07570900 17

FALL		63 N	66 JE	*00089652 AMEAN	*01184406 SIGMA
29 N		25 N	JE	*00072779 AMEAN	*03187706 SIGMA
*074529973823		-0.298053874036E-04		*675775141757E-07	-.323187646035E-04
-.110701869053E-06		.07265000	16		
473 N	483 JE		*00057329 AMEAN		*01183236 SIGMA
202 N	202 JE		*00025734 AMEAN		*02593735 SIGMA
*074470020403	-.303310851642E-04		*424962721334E-07		-.326282530301E-04
-.108744669638E-06	.07341500	19			
558 N	575 JE		*00042831 AMEAN		*00967863 SIGMA
252 N	252 JE		*00096085 AMEAN		*02890084 SIGMA
*075196633828	-.307456039839E-04		*387826647628E-07		-.318198270188E-04
-.11893403614E-06	.07416000	20			
486 N	500 JE		*00041327 AMEAN		*01128679 SIGMA
196 N	197 JE		*00034275 AMEAN		*03069611 SIGMA
*076475725405	-.313048960551E-04		*394490967851E-07		-.351120056390E-04
-.896076790981E-07	.07494500	21			
513 N	532 JE		*00029409 AMEAN		*01134144 SIGMA
188 N	188 JE		*00070575 AMEAN		*02676650 SIGMA
*077303846377	-.310324373275E-04		*56525057697E-07		-.364050371350E-04
-.770845504180E-07	.07570900	22			
233 N	249 JE		*00055684 AMEAN		*01366360 SIGMA
100 N	101 JE		*00136592 AMEAN		*03400048 SIGMA
*078009883524	-.307006562986E-04		*808690673004E-07		-.381294677370E-04
-.597978694152E-07	.07647400	23			
STATION V 00HRS GM1 SEASONS COMBINED					
224 N	227 JE		*00066458 AMEAN		*00693522 SIGMA
111 N	111 JE		*00104679 AMEAN		*02385175 SIGMA
*073742726211	-.295084259006E-04		*509910915601E-07		-.294580426772E-04
-.141212329378E-06	.07265000	1			
548 N	550 JE		*00038254 AMEAN		*00960745 SIGMA

250 N 250 JE * 00096174 AMEAN * 01055027 SIGMA
 * 074265321915 - .296404591366E-04 -.552296924611E-07 -.303731981129E-04
 -.137345456073E-06 .07341500 2
 463 N 467 JE * 00010092 AMEAN * 00091575 SIGMA
 192 N 192 JE * 00112189 AMEAN * 02786104 SIGMA
 * 074566129060 -.302857871537E-04 -.433444133352E-07 -.311252305886E-04
 -.129308750209E-06 .07418000 3
 493 N 497 JE * 00024288 AMEAN * 00947701 SIGMA
 216 N 221 JE * 00062345 AMEAN * 04046570 SIGMA
 * 075483116503 -.317409426338E-04 -.465518593752E-07 -.348111024533E-04
 -.951991274713E-07 .07494500 4
 477 N 495 JE * 00037819 AMEAN * 01217347 SIGMA
 204 N 205 JE * 00052841 AMEAN * 03139579 SIGMA
 * 076819784822 -.310082842379E-04 -.537445699170E-07 -.367416884154E-04
 -.756635078414E-07 .07570900 5
 503 N 543 JE * 00045160 AMEAN * 01605234 SIGMA
 184 N 184 JE -.00065091 AMEAN * 03406634 SIGMA
 * 0777727660911 -.306318303699E-04 -.8417160006234E-07 -.382500798133E-04
 -.577647836360E-07 .07647400 6
 446 N 512 JE * 00028312 AMEAN * 01638828 SIGMA
 187 N 187 JE -.00104431 AMEAN * 04069482 SIGMA
 * 079205506138 -.322837087475E-04 -.484228059255E-07 -.443498196073E-04
 -.207590944958E-07 .07723900 7
 186 N 209 JE * 00046880 AMEAN * 01594894 SIGMA
 64 N 64 JE * 00042416 AMEAN * 03378212 SIGMA
 * 080135279840 -.333287227749E-04 -.314208332089E-07 -.417557878261E-04
 -.398084367770E-07 .07600300 8

STATION V 12HR FOUR SEASONS

WINTER
 285 N 317 JE * 00030677 AMEAN * 01389208 SIGMA
 102 N 102 JE * 00101340 AMEAN * 02943109 SIGMA
 * 075624332070 -.286980828583E-04 -.115006992028E-06 -.366286477706E-04
 -.787878194283E-07 .07494500 1

519 N	576 JE	* 00020244	AMEAN	* 01463718 SIGMA
193 N	193 JE	* 00103998	AMEAN	* 02591571 SIGMA
* 076592440859	- .290187241174E-04	- .123699243857E-06	- .395272506162E-04	
- .503765266151E-07	.07570900	2		
509 N	579 JE	* 00004082	AMEAN	* 01632378 SIGMA
152 N	152 JE	- * 00211796	AMEAN	* 02925557 SIGMA
* 076091441643	- .303107641353E-04	- .109506561549E-06	- .391140301400E-04	
- .525701389808E-07	.07647400	3		
570 N	625 JE	* 00003183	AMEAN	* 01599494 SIGMA
195 N	195 JE	* 00041099	AMEAN	* 03893443 SIGMA
* 079076166276	- .305058446441E-04	- .117209079059E-06	- .370609323949E-04	
- .633789232041E-07	.07723900	4		
182 N	204 JE	- * 00006701	AMEAN	* 01797914 SIGMA
94 N	94 JE	- * 00157198	AMEAN	* 03135920 SIGMA
* 079311925241	- .320815241337E-04	- .558804140712E-07	- .457126158970E-04	
- .131787896224E-07	.07800300	5		
 SPRING				
300 N	303 JE	- * 00021213	AMEAN	* 00930673 SIGMA
85 N	85 JE	* 001571453	AMEAN	* 02060211 SIGMA
* 074230130565	- .298791450222E-04	- .534506280013E-07	- .277019360474E-04	
- .1613066253039E-06	.07418000	6		
543 N	548 JE	* 00005107	AMEAN	* 00703155 SIGMA
206 N	206 JE	* 00009827	AMEAN	* 03336226 SIGMA
* 075190085455	- .305547370120E-04	- .419669367707E-07	- .3414220992138E-04	
- .101092077309E-06	.07494500	7		
487 N	496 JE	- * 00008614	AMEAN	* 00936743 SIGMA
164 N	164 JE	* 00007403	AMEAN	* 02716496 SIGMA
* 076059077338	- .309897347071E-04	- .382261335649E-07	- .351303490689E-04	
- .969264363965E-07	.07570900	8		
526 N	533 JE	* 00023203	AMEAN	* 00942645 SIGMA
218 N	218 JE	* 00054277	AMEAN	* 02378035 SIGMA
* 076812831082	- .314493026731E-04	- .304295412045E-07	- .390781476125E-04	
- .584487887916E-07	.07647400	9		
542 N	565 JE	* 00063635	AMEAN	* 01231613 SIGMA
221 N	221 JE	- .00032297	AMEAN	* 02670419 SIGMA

* 078348772632 - .329248708264E-04 - .965242606402E-08 -.398181269436E-04
 - .553552965304E-07 10
 143 N 159 JE * 07723900 AMEAN * 01714368 SIGMA
 51 N 51 JE -.00224066 AMEAN * 02688810 SIGMA
 - .079480793954 -.331029840753E-04 -.228922596025E-07 -.390172357285E-04
 - .588398704511E-07 .07800300 11

SUMMER
 126 N 127 JE * 00023698 AMEAN * 00413199 SIGMA
 38 N 31 JE * 00105025 AMEAN * 01445720 SIGMA
 * 073355349458 -.292781907647E-04 -.600468763146E-07 -.289717760913E-04
 - .154414768880E-06 .07265000 12
 604 N 607 JE * 00030155 AMEAN * 00915839 SIGMA
 216 N 216 JE * 00168599 AMEAN * 02121952 SIGMA
 * 074245712057 -.297030779395E-04 -.545794300023E-07 -.296797941819E-04
 - .144049673135E-06 .07341500 13
 547 N 548 JE * 00005213 AMEAN * 00795139 SIGMA
 176 N 176 JE * 00167458 AMEAN * 02182120 SIGMA
 * 074593316277 -.302018333619E-04 -.438049492357E-07 -.2898880035472E-04
 - .153736994234E-06 .07418000 14
 195 N 196 JE -.0023128 AMEAN * 00884931 SIGMA
 46 N 46 JE * 00218660 AMEAN * 02346676 SIGMA
 * 075784831336 -.312511926059E-04 -.307202293925E-07 -.298732976122E-04
 - .142391587713E-06 .07494500 15

FALL
 220 N 221 JE * 00037170 AMEAN * 00686836 SIGMA
 72 N 72 JE * 00053397 AMEAN * 02929456 SIGMA
 * 074150371571 -.298353277870E-04 -.522245911671E-07 -.315744162615E-04
 - .120286746520E-06 .07341500 15
 504 N 593 JE * 00029615 AMEAN * 00811517 SIGMA
 196 N 198 JE * 00029319 AMEAN * 01879306 SIGMA
 * 074767015987 -.303353314597E-04 -.416035915692E-07 -.3220019293801E-04
 - .114552776729E-06 .07418000 17
 550 N 566 JE * 00008180 AMEAN * 01445630 SIGMA

171 N 172 JE -0.00099932 AMEAN • 03163100 SIGMA
 • 076526226097 -.315506128979E-04 -320686020215E-07 -.336927796765E-04
 -.101684380686E-06 .07494500 18
 466 N 505 JE -0.00028139 AMEAN • 01887042 SIGMA
 170 N 170 JE • 00052249 AMEAN • 02430470 SIGMA
 • 077353337808 -.318795221012E-04 -295590629490E-07 -.382940424519E-04
 -.656092084631E-07 .07570900 19
 155 N 166 JE • 00013526 AMEAN • 01594979 SIGMA
 74 N 74 JE -0.00215964 AMEAN • 03295328 SIGMA
 • 0780080812927 -.310313464471E-04 -.653790474402E-07 -.417386199709E-04
 -.321056579520E-07 .07647400 20

STATION V 12HR GMT SEASONS COMBINED

196 N	199 JE	• 00014989 AMEAN	• 00881123 SIGMA
52 N	52 JE	-0.00130513 AMEAN	• 03787252 SIGMA
• 073916084886 -.299941326198E-04		-0.512751042208E-07	-.326702082618E-04
-.110910166248E-06		.07265000 1	
606 N	606 JE	• 00005083 AMEAN	• 00553411 SIGMA
223 N	223 JE	• 00145157 AMEAN	• 02018565 SIGMA
• 074344613703 -.2999237524076E-04		-491276302453E-07	-.306214146130E-04
-.132444009455E-06		.07341500 2	
553 N	558 JE	• 00002111 AMEAN	• 08915739 SIGMA
136 N	136 JE	• 00145313 AMEAN	• 02055577 SIGMA
• 074615985705 -.300478828571E-04		-487287320771E-07	-.287255332136E-04
-.15407008624E-06		.07416000 3	
515 N	524 JE	• 00005604 AMEAN	• 00934670 SIGMA
190 N	191 JE	-0.0045776 AMEAN	• 03996293 SIGMA
• 075612650474 -.308948293335E-04		-411247744334E-07	-.352348123944E-04
-.897293631605E-07		.07494500 4	
502 N	541 JE	-0.0005692 AMEAN	• 01781205 SIGMA
154 N	154 JE	• 00036173 AMEAN	• 03583327 SIGMA
• 076479454601 -.309778902949E-04		-488600248723E-07	-.391820661612E-04
-.591521615776E-07		.07570900 5	
511 N	554 JE	-0.0003103 AMEAN	• 01597897 SIGMA
162 N	162 JE	-0.0126697 AMEAN	• 03087900 SIGMA
• 077362991056 -.309130357396E-04		-660007329740E-07	-.390862048701E-04

- .50 3331035570E-07	.07647488		
530 N	613 JE	* 080 31629	AMEAN
208 N	210 JE	* 080 43205	AMEAN
* 078605242681	- .308837050478E-04	- .918561324970E-07	- .386665155905E-04
* 526174600366E-07	.07723980		
230 N	250 JE	* 080 27643	AMEAN
90 N	90 JE	- * 08237092	AMEAN
* 079803779345	- .324815477912E-04	- .548742909066E-07	- .449476121309E-04
- .177757622013E-07	.07800300		

STATION D 00HR FOUR SEASONS

WINTER

202 N	203	JE	.00017445	AMEAN	.00795148 SIGMA
55 N	55	JE	-.01137327	AMEAN	.02505585 SIGMA
• 075201199460	-.290747156754E-04		-.960909371982E-07		-.491624571050E-04
• 128203755981E-07	.07494500		1		
566 N	565	JE	.00032453	AMEAN	.01221101 SIGMA
250 N	250	JE	-.00095379	AMEAN	.03567010 SIGMA
• 076209924511	-.302175594007E-04		-.762590474069E-07		-.499645097517E-04
• 135107672269E-07	.07570900		2		
647 N	696	JE	.00005214	AMEAN	.01592157 SIGMA
209 N	214	JE	-.00079727	AMEAN	.04651559 SIGMA
• 076900092343	-.297318476159E-04		-.998512339638E-07		-.456948677989E-04
• 127959762734E-07	.07647400		3		
651 N	676	JE	.00035674	AMEAN	.01337308 SIGMA
196 N	199	JE	-.00047310	AMEAN	.03863474 SIGMA
• 077913812130	-.313971154573E-04		-.486401006075E-07		-.467132054156E-04
• 405450322190E-08	.07723900		4		
601 N	662	JE	.00062950	AMEAN	.01782020 SIGMA
272 N	275	JE	-.00011937	AMEAN	.04359514 SIGMA
• 078642416241	-.300762517468E-04		-.113385451167E-06		-.457661220678E-04
• 111375163742E-07	.07800300		5		
615 N	672	JE	.00060939	AMEAN	.01632273 SIGMA
260 N	263	JE	-.00270465	AMEAN	.04367981 SIGMA
• 079821689538	-.314446922648E-04		-.857169991866E-07		-.466738593932E-04
• 624645074843E-08	.07876800		6		
612 N	686	JE	.00027257	AMEAN	.01592085 SIGMA
222 N	225	JE	-.00244308	AMEAN	.03884276 SIGMA
• 081422814858	-.328373602449E-04		-.659935324546E-07		-.493557037266E-04
• 100500760010E-07	.07953390		7		
147 N	160	JE	.00024923	AMEAN	.01663688 SIGMA
59 N	60	JE	-.00471553	AMEAN	.03700902 SIGMA
• 081991710164	-.335173208507E-04		-.364176559349E-07		-.545142973373E-04
• 375759098509E-07	.08030000		8		

SPRING						
697	N	705	JE	.00001826	AMEAN	.00004568 SIGMA
262	N	263	JE	-.00019727	AMEAN	.00051942 SIGMA
$\cdot 075982188328 - .299702669149E-84$						
$-.227176979176E-07$						
658	N	662	JE	.00022929	AMEAN	.00779777 SIGMA
292	N	292	JE	.00183909	AMEAN	.02046675 SIGMA
$.07649770574 -.306487084592E-04$						
$-.305971782366E-07$						
678	N	690	JE	.00065131	AMEAN	.01185496 SIGMA
282	N	282	JE	.00004972	AMEAN	.03492715 SIGMA
$.077739578662 -.312147204712E-04$						
$-.187751107567E-08$						
583	N	595	JE	.00073546	AMEAN	.01159167 SIGMA
279	N	280	JE	-.00112547	AMEAN	.03196412 SIGMA
$.070398003466 -.322587317971E-04$						
$-.680950634553E-08$						
201	N	204	JE	.00121485	AMEAN	.000875655 SIGMA
83	N	83	JE	-.00264956	AMEAN	.026664039 SIGMA
$.079036780259 -.329132182930E-04$						
$-.203057602270E-07$						
67	N	67	JE	.00006319	AMEAN	.00550582 SIGMA
242	N	242	JE	.00209705	AMEAN	.02516436 SIGMA
$.074969594627 -.305047060707E-04$						
$-.759892016452E-07$						
689	N	692	JE	.00017126	AMEAN	.00738451 SIGMA
276	N	276	JE	.00131022	AMEAN	.02410012 SIGMA
$.075490655603 -.300823446374E-04$						
$-.718087206402E-07$						
667	N	673	JE	.00046256	AMEAN	.000843615 SIGMA
234	N	234	JE	.00078373	AMEAN	.03056944 SIGMA
$.076279868693 -.306946496876E-04$						
$-.578053413702E-07$						
701	N	705	JE	.00044688	AMEAN	.00051068 SIGMA

270 N 270 JE .00001311 AMEAN .02920657 SIGMA
 • 077436565661 -.324678357697E-04 -.424573305965E-06 -.407746595068E-04
 -.519912791908E-07 .0/647400 17

FALL		127 N	130 JE	.00006332 AMEAN	.00 804976 SIGMA
51 N		51 N	51 JE	.00042924 AMEAN	.01921827 SIGMA
• 674513790840	-.	• 281427146752E-04		-114849322489E-06	-456952206212E-04
-.	110373459218E-07		.07418000 18		
57 ₄ N	58 ₇ JE		.00009833 AMEAN	.01020188 SIGMA	
214 N	214 JE		.00116902 AMEAN	.04111387 SIGMA	
• 075289849626	-.	• 293700160556E-04		-032618361345E-07	-415458514951E-04
-.	426769294118E-07		.07494500 19		
692 N	710 JE		.00008485 AMEAN	.00973025 SIGMA	
219 N	219 JE		.00000905 AMEAN	.03748946 SIGMA	
• 076267439288	-.	• 303959040614E-04		-588657804861E-07	-41884904645E-04
-.	40 992912611E-07		.07570900 20		
665 N	666 JE		.00047698 AMEAN	.01222738 SIGMA	
282 N	285 JE		.00100485 AMEAN	.04031502 SIGMA	
• 077242774614	-.	• 309923111008E-04		-506504126904E-07	-440222591979E-04
-.	258050625642E-07		.07647400 21		
685 N	696 JE		.00047447 AMEAN	.01093540 SIGMA	
247 N	251 JE		.00151753 AMEAN	.03649158 SIGMA	
• 078626273706	-.	• 330018932578E-04		-150243854752E-07	-470429172136E-04
-.	616213330289E-06		.07723900 22		
463 N	490 JE		.00026837 AMEAN	.01474414 SIGMA	
136 N	140 JE		.002223830 AMEAN	.04534904 SIGMA	
• 079786041844	-.	• 327418318176E-04		-385140908387E-07	-458347364658E-04
-.	133804609540E-07		.07800300 23		
232 N	237 JE		.00014125 AMEAN	.01103572 SIGMA	
94 N	94 JE		.00346199 AMEAN	.03080120 SIGMA	
• 081084339323	-.	• 356381647524E-04		403034286791E-07	-510665115701E-04
-.	143 51788132E-07		.07876800 24		

STATION D 00HR GMT SEASONS COMBINED
 102 N 102 JE .00011239 AMEAN .00724097 SIGMA

51 N 51 JE *00124714 AMEAN *01695610 SIGMA
 *073979445476 -.302712074454E-04 -440561089766E-07 -.379174319098E-04
 -.683772625809E-07 .07341500 1
 685 N 695 JE *000080386 AMEAN *009248660 SIGMA
 239 N 249 JE *00068748 AMEAN *04539054 SIGMA
 *074682535850 -.297035064226E-04 -.664535400846E-07 -.396628988410E-04
 -.565749764122E-07 .07410000 2
 657 N 665 JE -.00004133 AMEAN *00796397 SIGMA
 253 N 255 JE *00118412 AMEAN *03500768 SIGMA
 *075575819316 -.303915252036E-04 -.496792772127E-07 -.384794088793E-04
 -.681120246631E-07 3
 692 N 709 JE *00015133 AMEAN *00973602 SIGMA
 244 N 251 JE -.00030336 AMEAN *04513063 SIGMA
 *076223204820 -.302030861720E-04 -.612360403510E-07 -.414820141261E-04
 -.437664639842E-07 .07570900 4
 702 N 723 JE *00019145 AMEAN *01201187 SIGMA
 278 N 286 JE *00014462 AMEAN *03981874 SIGMA
 *077073463784 -.308710441991E-04 -.509744863712E-07 -.436832236911E-04
 -.284257466426E-07 .07647400 5
 666 N 680 JE *00043718 AMEAN *00987463 SIGMA
 264 N 264 JE -.00084249 AMEAN *02955455 SIGMA
 *077633998787 -.31647171787E-04 -.3448564485515E-07 -.495702127057E-04
 *.884999950345E-06 .07723900 6
 631 N 666 JE *00047499 AMEAN *01416375 SIGMA
 263 N 272 JE *00229513 AMEAN *04176764 SIGMA
 *079107665996 -.320999149108E-04 -.473864353122E-07 -.482303704820E-04
 *.289688176300E-08 .07800300 7
 629 N 683 JE *00059020 AMEAN *01622123 SIGMA
 251 N 255 JE *00239037 AMEAN *04196134 SIGMA
 *079944624730 -.324052045820E-04 -.52319186652E-07 -.491021792742E-04
 *.750858512163E-08 .07876208 8
 613 N 687 JE *00051533 AMEAN *01594620 SIGMA
 239 N 245 JE *00194374 AMEAN *03950906 SIGMA
 *081089156750 -.328678362293E-04 -.565750788939E-07 -.493951123231E-04
 *.107113888380E-07 .07953300 9
 169 N 183 JE *00027336 AMEAN *01611073 SIGMA

60 N 61 JE - .86472267 AMEAN * 03755674 SIGMA
 * 001000292213 - .33667531663E-04 -.293347044346E-07 -.551969779364E-04
 * 40 0634636773E-07 .06030008 10

STATION D 12HR FOUR SEASONS

WINTER		SUMMER		AUTUMN		SPRING	
245 N	252 JE	000 20 543	AMEAN	010 757 30	SIGMA	010 757 30	SIGMA
76 N	76 JE	- 001 00 414	AMEAN	022 482 02	SIGMA		
* 075696723767	- .296927579965E-04	- .9378956666281E-07	- .486743066601E-04				
* 666940660293E-08	.07494500	1					
570 N	594 JE	- 000 01 0631	AMEAN	011 027 02	SIGMA		
211 N	214 JE	- 00151847	AMEAN	03822676	SIGMA		
* 076045751111	- .286210650855E-04	- .127122912961E-06	- .470241082587E-04				
- .704226826954E-09	.07570900	2					
572 N	586 JE	- 0010630	AMEAN	01 281770	SIGMA		
245 N	252 JE	- 000 09019	AMEAN	04 387340	SIGMA		
* 077259886996	- .304970244682E-04	- .739845416645E-07	- .4703 84723104E-04				
- .382941112750E-08	.07647400	3					
610 N	652 JE	- 000 45741	AMEAN	01577219	SIGMA		
274 N	275 JE	- 000 27503	AMEAN	04202107	SIGMA		
* 077699973561	- .302034034172E-04	- .901166413743E-07	- .463424988997E-04				
- .032498267076E-08	.07723900	4					
599 N	657 JE	- 000 48676	AMEAN	01607011	SIGMA		
287 N	286 JE	- 00102863	AMEAN	03846283	SIGMA		
* 078947603181	- .308109303553E-04	- .961857063851E-07	- .483569760312E-04				
* 603486348781E-08	.07800300	5					
580 N	666 JE	- 000 79728	AMEAN	01760286	SIGMA		
233 N	237 JE	- 00109451	AMEAN	03921580	SIGMA		
* 079682994294	- .314227117251E-04	- .637977888897E-07	- .495772900225E-04				
* 132230390100E-07	.07076800	6					
496 N	536 JE	- 000 50122	AMEAN	01518017	SIGMA		
186 N	186 JE	- 00322845	AMEAN	03814613	SIGMA		
* 080746972925	- .316811749629E-04	- .859430568349E-07	- .516088154792E-04				
* 239024257528E-07	.07953300	7					

255 N 260 JE .00051776 AMEAN .01113911 SIGMA
 96 N 96 JE -.00397670 AMEAN .02553956 SIGMA
 .062405784303 -.34737196 0970E-04 -.466387019041E-06 -.543409476729E-04
 .33 6993037232E-07 .08030000 8

SPRING

403 N	417 JE	.00020368 AMEAN	.01062315 SIGMA
189 N	192 JE	-.00144651 AMEAN	.04073963 SIGMA
.075044109371	-.288563190972E-06	-.101593848890E-06	-.448553373763E-04
-.161971917202E-07	.07494500	9	
635 N	635 JE	-.0002202 AMEAN	.00 052228 SIGMA
272 N	272 JE	.00030354 AMEAN	.03410877 SIGMA
.076100040134	-.298719156259E-04	-.743126936749E-07	-.458586213209E-04
-.128445508091E-07	.07570900	10	
659 N	665 JE	.00052909 AMEAN	.00944259 SIGMA
315 N	317 JE	.00124044 AMEAN	.03320826 SIGMA
.076716776518	-.307249494268E-04	-.515915733920E-07	-.437925081029E-04
-.287519954136E-07	.07647400	11	
663 N	675 JE	.00067663 AMEAN	.01022552 SIGMA
314 N	314 JE	-.00035225 AMEAN	.03555745 SIGMA
.077482199658	-.311805104180E-04	-.463571132521E-07	-.469088142786E-04
-.608255232731E-08	.07723900	12	
639 N	651 JE	.00101609 AMEAN	.01230473 SIGMA
270 N	273 JE	-.0008199 AMEAN	.03253444 SIGMA
.078277689904	-.322321307668E-04	-.247620136957E-07	-.473306105450E-04
-.663328793135E-08	.07800300	13	
251 N	264 JE	.00096984 AMEAN	.01218156 SIGMA
120 N	120 JE	-.0012967 AMEAN	.02919966 SIGMA
.079551330863	-.335096886654E-04	.941510732266E-10	-.501753848106E-04
115324999673E-07	.07876800	14	

SUMMER

115 N	115 JE	.00010428 AMEAN	.00503920 SIGMA
50 N	50 JE	.00165638 AMEAN	.02100200 SIGMA
.074212112946	-.298054670778E-06	-.608736758428E-07	-.377735791430E-04
-.711009701389E-07	.07341500	15	

658 N	658 JE	*.00021064	A MEAN	*.00626715 SIGMA
280 N	280 JE	*.08117701	A MEAN	*.02372541 SIGMA
*.074962523778	-.301041376707E-04	-.5266680054073E-07	-.392155793939E-04	
-*.601031392696E-07	.07416800	16		
622 N	629 JE	*.00030950	A MEAN	*.00757546 SIGMA
253 N	253 JE	*.00195630	A MEAN	*.02831583 SIGMA
*.075626273937	-.3046930156589E-04	-.481856923327E-07	-.372848474903E-04	
-*.7770408644900E-07	.07494500	17		
653 N	653 JE	*.00069009	A MEAN	*.00743414 SIGMA
253 N	253 JE	*.0076047	A MEAN	*.02047481 SIGMA
*.076410104654	-.313068666525E-04	-.260364145673E-07	-.391995701413E-04	
-*.630318044199E-07	.07570900	18		
695 N	701 JE	*.00076420	A MEAN	*.00993039 SIGMA
281 N	281 JE	*.00076539	A MEAN	*.03112714 SIGMA
*.077231803078	-.318277364320E-04	-.232135557289E-07	-.405036936893E-04	
-*.514463283211E-07	.07647400	19		
 FALL				
288 N	289 JE	*.0002769	A MEAN	*.00629417 SIGMA
131 N	131 JE	-.0007733	A MEAN	*.03029892 SIGMA
*.074702463755	-.295728962160E-04	-.755680302420E-07	-.442471655223E-04	
-*.225039431792E-07	.07418000	20		
601 N	611 JE	*.00019601	A MEAN	*.00922337 SIGMA
275 N	275 JE	*.00061465	A MEAN	*.03463331 SIGMA
*.075623162903	-.302091588067E-04	-.617721728559E-07	-.430336707028E-04	
-*.318496604062E-07	.07494500	21		
619 N	625 JE	*.00019251	A MEAN	*.00649939 SIGMA
277 N	277 JE	*.00062156	A MEAN	*.03110796 SIGMA
*.076096133738	-.305355209281E-04	-.497897996839E-07	-.423664381247E-04	
-*.350914987815E-07	.07570900	22		
616 N	637 JE	*.00042148	A MEAN	*.01134444 SIGMA
244 N	245 JE	*.0006509	A MEAN	*.03576894 SIGMA
*.077300465867	-.317215272635E-04	-.290137114986E-07	-.450572113957E-04	
-*.210260500949E-07	.07647400	23		
581 N	599 JE	*.00057282	A MEAN	*.01213544 SIGMA
251 N	252 JE	-.00021597	A MEAN	*.03641984 SIGMA

• 078374222534 - .321386131371E-04 - .341790866952E-07 - .459166588456E-04
 - .133659375145E-07 .07723900 24
 504 N 523 JE .00058396 AMEAN • 01280552 SIGMA
 190 N 190 JE -.00286646 AMEAN • 03233628 SIGMA
 • 079450197125 -.331145560273E-04 -.156423351578E-07 -.482443095251E-04
 • 824376717580E-09 .07800300 25
 238 N 246 JE .00069645 AMEAN • 01513175 SIGMA
 73 N 73 JE .00107205 AMEAN • 03973437 SIGMA
 • 080253098401 -.330941080365E-04 -.332928806894E-07 -.454886158652E-04
 - .176261962349E-07 .07876800 26

STATION 0 12 HR GMT SEASONS COMBINED
 129 N 129 JE .00028562 AMEAN • 01649157 SIGMA
 50 N 50 JE .00160527 AMEAN • 02089677 SIGMA
 • 073947459705 -.297475484235E-04 -.613793362679E-07 -.379134215541E-04
 - .700848771960E-07 .07341500 1
 645 N 64 JE .00025545 AMEAN • 00797880 SIGMA
 268 N 26 JE .00059627 AMEAN • 02974363 SIGMA
 • 075037773768 -.301867326750E-04 -.544953975909E-07 -.391665897824E-04
 - .599752474604E-07 .07418000 2
 606 N 624 JE .00004016 AMEAN • 01011612 SIGMA
 286 N 286 JE -.00010005 AMEAN • 04278541 SIGMA
 • 075794907465 -.304581634864E-04 -.579937745210E-07 -.40104632266E-04
 - .533733688017E-07 .07494500 3
 603 N 611 JE .00033465 AMEAN • 01114166 SIGMA
 252 N 260 JE .00010543 AMEAN • 04261765 SIGMA
 • 076431693417 -.303604202217E-04 -.452009365736E-07 -.4256194863633E-04
 - .358610591716E-07 .07570900 4
 627 N 643 JE .00065522 AMEAN • 00999630 SIGMA
 275 N 275 JE .00078709 AMEAN • 03442630 SIGMA
 • 076833579646 -.311245839960E-04 -.407364048835E-07 -.430660866528E-04
 - .277739740326E-07 .07647400 5
 629 N 640 JE .00043754 AMEAN • 01284562 SIGMA
 299 N 301 JE -.00005196 AMEAN • 04127314 SIGMA
 • 077647641755 -.310449587155E-04 -.525758297977E-07 -.463573941307E-04
 - .115294993514E-07 .07723900 6

611 N	659 JE	.00056601	AMEAN	.01533323 SIGMA
262 N	265 JE	-.00229007	AMEAN	.04311119 SIGMA
*.078832795282	-.309978824237E-04	-.799879745070E-07		-.478567255843E-04
*.882893395758E-09	.07800300	7		
579 N	660 JE	.00079341	AMEAN	.01832358 SIGMA
237 N	241 JE	-.00102545	AMEAN	.04138472 SIGMA
*.0796667559885	-.317473686701E-04	-.691300877586E-07		-.480452745885E-04
*.528108716149E-08	.07876800	8		
557 N	606 JE	.00067609	AMEAN	.01593925 SIGMA
209 N	216 JE	-.00195685	AMEAN	.04470457 SIGMA
*.080841350228	-.321567148260E-04	-.734357462963E-07		-.485759732423E-04
*.576107126228E-08	.07953300	9		
316 N	324 JE	.00064744	AMEAN	.01164233 SIGMA
128 N	128 JE	-.00364582	AMEAN	.02470810 SIGMA
*.082176321242	-.344272633121E-04	-.117160203563E-07		-.545775692865E-04
*.373347423114E-07	.08030000	10		

STATION N 00HR FOUR SEASONS

WINTER						
345	N	35° JE	.00046704	AMEAN	.81277273 SIGMA	
100	N	100 JE	.00035050	AMEAN	.03305066 SIGMA	
*07493257	3411	..209664839751E-04	- .9070626140	42E-07	-.401320092619E-04	
-0.432496420354E-07		*07416000	¹			
404	N	424 JE	.00093351	AMEAN	.01350650 SIGMA	
130	N	130 JE	.00033612	AMEAN	.03230926 SIGMA	
*075821804059	..304773527736E-04	- .549714751728E-07	-.371139856056E-04			
-0.695240263965E-07		.07494500	²			
529	N	544 JE	.00064400	AMEAN	.01022277 SIGMA	
214	N	214 JE	-.00094971	AMEAN	.02771327 SIGMA	
*076774683103	..310458698615E-04	- .402242185578E-07	-.411085019938E-04			
-0.408129281402E-07		.07570900	³			
476	N	488 JE	.00048655	AMEAN	.01159683 SIGMA	
207	N	207 JE	-.00191957	AMEAN	.02523630 SIGMA	
*077507358099	..310505861373E-04	- .425443860768E-07	-.457557943174E-04			
-0.119070622443E-07		.07647400	⁴			
257	N	260 JE	.00018189	AMEAN	.01061343 SIGMA	
115	N	115 JE	-.00035825	AMEAN	.02473042 SIGMA	
*077929503260	..306917238119E-04	- .5596835190	77E-07	-.451326136383E-04		
-0.149642714959E-07		.07723900	⁵			
SPRING						
76	N	76 JE	.00035731	AMEAN	.00561433 SIGMA	
36	N	36 JE	.00142004	AMEAN	.02450052 SIGMA	
*075656015018	..315169202752E-04	- .172611994834E-07	-.360314804333E-04			
-0.870703099174E-07		*07416000	⁶			
391	N	395 JE	.00114896	AMEAN	.00933454 SIGMA	
159	N	159 JE	.00062977	AMEAN	.02508924 SIGMA	
*075707743701	..308268027213E-04	- .324142943320E-07	-.367173603616E-04			
-0.811608589937E-07		.07494500	⁷			
415	N	417 JE	.00107564	AMEAN	.00790353 SIGMA	
190	N	191 JE	.00168097	AMEAN	.02531245 SIGMA	
*0765309955003	..320358221026E-04	- .571234535200E-06	-.395916039205E-04			

-.587602122498E-07 * 07570900
 473 N 477 JE * 00062862 AMEAN * 00965470 SIGMA
 216 N 216 JE * 00071256 AMEAN * 02587751 SIGMA
 * 077975240890 -.332043337042E-04 .141194064681E-07 -.414836035365E-04
 -479817391152E-07 .07647400 9

8

SUMMER

86 N	86 JE	* 00050511 AMEAN	* 01697220 SIGMA
38 N	32 JE	- 00013753 AMEAN	* 01937327 SIGMA
* 075535259549	-.309685695473E-04	- 306198727746E-07	-.366148693386E-04
-77711141469E-07	.07341500	10	
499 N	500 JE	* 00065237 AMEAN	* 00881852 SIGMA
210 N	210 JE	- 00036426 AMEAN	* 01657734 SIGMA
* 075730182801	-.3169802028105E-04	- 661927279529E-08	-.373989493867E-04
-732340776367E-07	.07416000	11	
509 N	512 JE	* 00067512 AMEAN	* 00786210 SIGMA
225 N	225 JE	* 00033057 AMEAN	* 01638805 SIGMA
* 0760266025917	-.321332465206E-04	* 221925538649E-08	-.372119981242E-04
-742153004065E-07	.07494500	12	
79 N	80 JE	* 00076989 AMEAN	* 00995070 SIGMA
47 N	47 JE	* 00050203 AMEAN	* 01360942 SIGMA
* 076855794453	-.327921631762E-04	.127480820621E-07	-.362235526017E-04
-833916604657E-07	.07570900	13	

FALL

509 N	517 JE	* 00090806 AMEAN	* 01095847 SIGMA
205 N	205 JE	- 00020505 AMEAN	* 02194951 SIGMA
* 075320852767	-.301301961779E-04	- 534707210572E-07	-.378152118514E-04
-67444076983E-07	.07418000	14	
509 N	514 JE	* 00053165 AMEAN	* 00785029 SIGMA
244 N	244 JE	- 00007612 AMEAN	* 01668371 SIGMA
* 076184221139	-.316049427799E-04	- 134210731908E-07	-.364000143082E-04
-656966906729E-07	.07494500	15	
514 N	514 JE	* 00054794 AMEAN	* 00849138 SIGMA
207 N	207 JE	* 0034522 AMEAN	* 01802577 SIGMA
* 077141206508	-.324277190137E-04	.211205060479E-08	-.3622398588320E-04

-0 702552948529E-07 .07570900
 298 N 301 JE .08053115 AMEAN .01060601 SIGMA
 114 N 110 JE -.00302350 AMEAN .03117406 SIGMA
 .077979461775 -.329876317293E-04 .003654016456E-06 -.419353872145E-04
 -.410690823436E-07 .07647400
 17

STATION N 00HR GNT SEASONS COMBINED
 193 N 196 JE .00059901 AMEAN .00778414 SIGMA
 01 N 61 JE .00140063 AMEAN .02737500 SIGMA
 .074772745343 -.292840188176E-04 -.769555847219E-07 -.3579818441708E-04
 .843081358996E-07 .07341500
 505 N 50 E JE .00077450 AMEAN .01012429 SIGMA
 225 N 225 JE .00080690 AMEAN .02065777 SIGMA
 .075441973594 -.309651835058E-04 -.269140521320E-07 -.371015521651E-04
 .7558066937952E-07 .07416000
 457 N 463 JE .00072367 AMEAN .01157901 SIGMA
 203 N 203 JE -.0008806 AMEAN .02272181 SIGMA
 .076083585197 -.316479053785E-04 -.148231771513E-07 -.369145982227E-04
 .758774223599E-07 .07494500
 471 N 478 JE .00056307 AMEAN .00063241 SIGMA
 201 N 201 JE .00060300 AMEAN .02609989 SIGMA
 .077107991364 -.32223521246000E-04 -.573989527846E-06 -.384291371919E-04
 -.600784658505E-07 .07570900
 494 N 501 JE .00068673 AMEAN .01046365 SIGMA
 220 N 220 JE -.00065669 AMEAN .03160519 SIGMA
 .077608343235 -.319793465455E-04 -.164267239312E-07 -.429934349899E-04
 .335113692327E-07 .07647400
 450 N 455 JE .00026036 AMEAN .01066220 SIGMA
 189 N 190 JE -.00045643 AMEAN .02525807 SIGMA
 .078143248904 -.311601577852E-04 -.425103792611E-07 -.467613205198E-04
 -.405214530445E-06 .07723900
 5

STATION N 12HR FOUR SEASONS

WINTER

253 N 266 JE * 00012515 AMEAN * 01324448 SIGMA
 52 N 52 JE * 00050380 AMEAN * 02652525 SIGMA
 * 074042105239 * 0.278788340110E-04 - 127590352902E-06 - .374373158199E-04
 -.667674470411E-07 .07418000 1
 434 N 441 JE * 00124579 AMEAN * 01613937 SIGMA
 142 N 142 JE * 00208673 AMEAN * 03966920 SIGMA
 * 075929740824 - 303605365220E-04 - 520655392390E-07 - 412316993071E-04
 405054530282E-07 2
 534 N 541 JE * 00039599 AMEAN * 01613934 SIGMA
 195 N 195 JE * 00111202 AMEAN * 0230670 SIGMA
 * 077734520967 - 321011291935E-04 - 104199269905E-07 - 432945122233E-04
 - 42623401209E-07 3
 538 N 553 JE * 00019871 AMEAN * 01149774 SIGMA
 186 N 186 JE * 00150558 AMEAN * 02524695 SIGMA
 * 076738432217 - 31214138030307E-04 - 357695097001E-07 - 411699824997E-04
 - 405054530282E-07 4
 545 N 562 N 573 JE * 00038629 AMEAN * 01613937 SIGMA
 196 N 196 JE * 00034443 AMEAN * 02644661 SIGMA
 * 077734520967 - 321011291935E-04 - 104199269905E-07 - 432945122233E-04
 - 301424653271E-07 5
 545 JE * 07647400 6
 538 JE * 00038629 AMEAN * 01613937 SIGMA
 209 N 209 JE * 00019871 AMEAN * 01149774 SIGMA
 * 070569654683 - 316913278125E-04 - 329570634335E-07 - 4080361450707E-04
 363203426825E-06 * 0.07723900 7
 SPRING
 435 N 436 JE * 00053366 AMEAN * 00022514 SIGMA
 171 N 171 JE * 00134851 AMEAN * 0235335 SIGMA
 * 075847480322 - 312871613980E-04 - 193255695740E-07 - 368794120407E-04
 - 810753583840E-07 8
 467 N 476 JE * 00075289 AMEAN * 0009087 AMEAN * 02761551 SIGMA
 168 N 168 JE * 0009087 AMEAN * 02761551 SIGMA
 * 076122676564 - 313609283261E-04 - 178844941807E-07 - 372978468853E-04
 - 813955281313E-07 9
 545 JE * 07570900 10
 45 N 45 JE * 0002663 AMEAN * 00022514 SIGMA
 21 N 21 JE * 00016645 AMEAN * 01187628 SIGMA
 * 0757987 SIGMA
 * 02299263 SIGMA
 * 102805036195E-07 - 419140461907E-04
 * 07569050569 - 321008135725E-04 - 102805036195E-07 - 419140461907E-04
 - 810753583840E-07 11
 420062806457E-07 12
 221 N 221 JE * 00055497 AMEAN * 0235335 SIGMA
 * 075847480322 - 312871613980E-04 - 193255695740E-07 - 368794120407E-04
 - 810753583840E-07 13
 467 N 476 JE * 00035642 AMEAN * 007647400 14
 171 N 171 JE * 00134851 AMEAN * 0235335 SIGMA
 * 075847480322 - 312871613980E-04 - 193255695740E-07 - 368794120407E-04
 - 810753583840E-07 15
 467 N 476 JE * 00075289 AMEAN * 0009087 AMEAN * 02761551 SIGMA
 168 N 168 JE * 0009087 AMEAN * 02761551 SIGMA
 * 076122676564 - 313609283261E-04 - 178844941807E-07 - 372978468853E-04
 - 813955281313E-07 16
 545 JE * 07570900 17
 45 N 45 JE * 0002663 AMEAN * 00022514 SIGMA
 21 N 21 JE * 00016645 AMEAN * 01187628 SIGMA
 * 0757987 SIGMA

TR 82-81

* 079056291264 -.337326096886E-04 .203471061346E-07 -.456574546014E-04
-0 154134699462E-07 .07723900 9

SUMMER

531 N	532 JE	.00034984	AMEAN	.00660680 SIGMA
199 N	19 $\frac{1}{2}$ JE	.00022131	AMEAN	.01750167 SIGMA
* 075195491347	-.3000611200996E-04	-.245752440530E-07		-.357351490062E-04
-0 070270900551E-07	.07410000	10		
595 N	597 JE	.00042195	AMEAN	.00820590 SIGMA
237 N	237 JE	-.00056185	AMEAN	.02051213 SIGMA
* 076142060438	-.310526175551E-04	-.778746103145E-06		-.373945922702E-04
-0 721054863622E-07	.07494500	11		
263 N	264 JE	.00036331	AMEAN	.00907915 SIGMA
114 N	114 JE	.00061468	AMEAN	.01597999 SIGMA
* 076938962304	-.329374171015E-04	.169217370051E-07		-.373712659650E-04
-0 766033659373E-07	.07570900	12		

FALL

521 N	527 JE	.00028236	AMEAN	.00789974 SIGMA
187 N	187 JE	-.00020016	AMEAN	.02351643 SIGMA
* 075515245795	-.300091972139E-04	-.339832307651E-07		-.372551586503E-04
-0 751015191009E-07	.07410000	13		
580 N	587 JE	.00029775	AMEAN	.00934041 SIGMA
242 N	242 JE	-.00035018	AMEAN	.02670535 SIGMA
* 0759105521053	-.308154601982E-04	-.344195501042E-07		-.38133336629006E-04
-0 674910099363E-07	.07494500	14		
591 N	595 JE	.00026909	AMEAN	.00843854 SIGMA
239 N	23 $\frac{1}{2}$ JE	-.00012962	AMEAN	.02980190 SIGMA
* 077219041680	-.321229246281E-04	-.775475155999E-08		-.4055580003617E-04
-0 546451515696E-07	.07570900	15		
483 N	493 JE	.00053540	AMEAN	.01010876 SIGMA
234 N	234 JE	-.00102617	AMEAN	.02268710 SIGMA
* 077541608354	-.324190161673E-04	-.256857871999E-06		-.420993310119E-04
-0 413863499833E-07	.07647400	16		

STATION N 12HR GMT SEASONS COMBINED

538 N 542 JE *00024575 AMEAN *00751044 SIGMA
 200 N 200 JE *00028534 AMEAN *02154154 SIGMA
 *075299761035 -. 307229523672E-04 -. 323276066511E-07 -. 364432945210E-04
 -. 816138323838E-07 .074160000 1
 550 N 560 JE *00019904 AMEAN *00798989 SIGMA
 198 N 200 JE *00078250 AMEAN *02750753 SIGMA
 *. 076029127723 -. 314262046169E-04 -. 157347405333E-67 -. 384523685198E-04
 -. 663887196135E-07 .07494500 2
 482 N 486 JE *00026024 AMEAN *01039125 SIGMA
 153 N 153 JE *00018146 AMEAN *02647167 SIGMA
 *. 076604744956 -. 315083000805E-04 -. 203766372661E-07 -. 385194270053E-04
 -. 696603225045E-07 .07570900 3
 569 N 575 JE *00034650 AMEAN *00989130 SIGMA
 213 N 213 JE *00000030 AMEAN *02258485 SIGMA
 *. 077768202898 -. 325445363147E-04 -. 877500014765E-09 -. 432113049894E-04
 -. 326195805065E-07 .07647400 4
 362 N 367 JE *00028249 AMEAN *01064500 SIGMA
 149 N 149 JE *00019117 AMEAN *02104073 SIGMA
 *. 078691408977 -. 325574661978E-04 -. 8555772750355E-06 -. 462939688556E-04
 -. 115366800166E-07 .07723900 5

STATION C 00HR FOUR SEASONS

WINTER

116 N	141	JE	* 00126 952	AMEAN	* 02177 890	SIGMA
57 N	62	JE	* 00211 216	AMEAN	* 06277 720	SIGMA
* 075360925297	-	* 27557222504E-04	-	* 200713475929E-06	-	* 413516053063E-04
- .37 2740240722E-07		.07494500				
171 N	190	JE	* 00051 293	AMEAN	* 0152 010	SIGMA
59 N	59	JE	- * 00331 024	AMEAN	* 01910 416	SIGMA
* 074775334714	-	* 258155391981E-04	-	* 2405020588 60E-06	-	* 489006589924E-04
* 138002095314E-07		.07570900				
581 N	616	JE	- * 00012704	AMEAN	* 01454 056	SIGMA
192 N	96	JE	- * 00400 198	AMEAN	* 04031 013	SIGMA
* 075971117835	-	* 287312048184E-04	-	* 135673319214E-06	-	* 504574631009E-04
* 168030006980E-07		.07647400				
546 N	595	JE	* 00027232	AMEAN	* 01748 873	SIGMA
218 N	220	JE	- * 0162203	AMEAN	* 04316 938	SIGMA
* 077106645223	-	* 295541198246E-04	-	* 123883678984E-06	-	* 504891189695E-04
* 157795253951E-07		.07723900				
536 N	604	JE	- * 00010 520	AMEAN	* 01915 953	SIGMA
172 N	179	JE	- * 00310 761	AMEAN	* 05272 502	SIGMA
* 077914884648	-	* 290628183349E-04	-	* 149349665417E-06	-	* 498376099007E-04
* 140946495449E-07		.07800300				
473 N	545	JE	* 00053707	AMEAN	* 01938 740	SIGMA
177 N	178	JE	- * 00206 350	AMEAN	* 03916 397	SIGMA
* 078874009513	-	* 297979857503E-04	-	* 138820377576E-06	-	* 478067214484E-04
* 214294550984E-06		.07876600				
536 N	597	JE	* 00016 121	AMEAN	* 01745 227	SIGMA
202 N	208	JE	- * 00058 131	AMEAN	* 04297706	SIGMA
* 080176842168	-	* 312679640321E-04	-	* 103212535107E-06	-	* 491983789699E-04
* 661117577379E-06		.07953300				
544 N	580	JE	* 00057 462	AMEAN	* 01424153	SIGMA
183 N	185	JE	- * 00210 043	AMEAN	* 04214261	SIGMA
* 081540630907	-	* 330672711686E-04	-	* 513902999155E-07	-	* 512787023508E-04
* 153135809295E-07		.08030000				

SPRING

112 N 119 JE * 00015276 AMEAN * 01263036 SIGMA
 40 N 40 JE * 00262058 AMEAN * 01634909 SIGMA
 * 075049432207 - .264739645731E-04 - .217119525372E-06 -.461637525465E-04
 * 615762691068E-08 .07570908 9
 397 N 431 JE * 00013708 AMEAN * 01602730 SIGMA
 133 N 133 JE * 00147809 AMEAN * 03584016 SIGMA
 * 076532932459 - .297199788035E-04 - .111711889434E-06 -.493093917482E-04
 * 151704953332E-07 .07647460 10
 528 N 557 JE * 00044136 AMEAN * 01383060 SIGMA
 198 N 198 JE * 00100500 AMEAN * 03423068 SIGMA
 * 076932026242 - .299919591061E-04 -.100326256716E-06 -.487317160567E-04
 * 115813422709E-07 .07723900 11
 611 N 643 JE * 00000036 AMEAN * 01453319 SIGMA
 238 N 238 JE * 00040533 AMEAN * 03649474 SIGMA
 * 077550899087 - .314220748153E-04 -.554447515007E-07 -.483063381137E-04
 * 336005104320E-08 .07800300 12
 573 N 597 JE * 00041183 AMEAN * 01498374 SIGMA
 198 N 201 JE * 00079198 AMEAN * 02786059 SIGMA
 * 078348449460 - .313220122889E-04 -.598990495202E-07 -.502270348586E-04
 * 151819968970E-07 .07876800 13
 467 N 535 JE * 00091901 AMEAN * 01749101 SIGMA
 160 N 166 JE * 00100230 AMEAN * 02964265 SIGMA
 * 080199647439 - .322069546225E-04 -.715872135145E-07 -.489754574673E-04
 * 856678871500E-08 .07953300 14
 348 N 375 JE * 00060149 AMEAN * 01559159 SIGMA
 113 N 115 JE * 00208809 AMEAN * 03854776 SIGMA
 * 080508429643 - .328822596616E-04 -.408991403385E-07 -.522967915027E-04
 * 204746085702E-07 .08030000 15

SUMMER

469 N 491 JE * 00021151 AMEAN * 01227337 SIGMA
 160 N 160 JE * 00131275 AMEAN * 02710242 SIGMA
 * 075144901493 - .289405409807E-04 -.114335727585E-06 -.456971494182E-04
 * 395641637973E-08 .07570900 16
 679 N 698 JE * 00012914 AMEAN * 01040297 SIGMA

226 N 226 JE -0.00142079 AMEAN .02710947 SIGMA
 • 076047052727 -0.301540011647E-04 -0.754052536400E-07 -0.472749372994E-04
 • 222060792569E-08 *07647400 17
 592 N 621 JE *00000582 AMEAN *01477647 SIGMA
 170 N 171 JE *00030270 AMEAN *03042247 SIGMA
 • 077100334003 -.312494979834E-04 -0.574327406769E-07 -0.451410062102E-04
 -0.167300992907E-07 18
 647 N 665 JE *00062791 AMEAN *01310128 SIGMA
 214 N 214 JE -0.00040739 AMEAN *03364650 SIGMA
 • 0773004929601 -.314225907145E-04 -0.472152672564E-07 -0.430910978062E-04
 -0.302630630547E-07 19
 412 N 437 JE *00077457 AMEAN *01227418 SIGMA
 163 N 163 JE -.00055041 AMEAN *03165494 SIGMA
 • 077705460101 -.321807373466E-04 -0.26809511126E-07 -0.637323282191E-04
 -0.286243545641E-07 20
 FALL
 159 N 167 JE .00025371 AMEAN *01244965 SIGMA
 52 N 52 JE -.00246044 AMEAN *01574213 SIGMA
 • 074051425143 -.264000134963E-04 -0.195214059219E-06 -0.475800686654E-04
 • 110569676027E-07 21
 126 N 141 JE *000037929 AMEAN *01574206 SIGMA
 52 N 52 JE -.000000878 AMEAN *02932760 SIGMA
 • 075236226109 -.276078246712E-04 -0.170896331347E-06 -0.476351770662E-04
 • 570707349096E-06 22
 622 N 665 JE *000000264 AMEAN *01510229 SIGMA
 216 N 217 JE *00004649 AMEAN *03950908 SIGMA
 221 N 221 JE -.00193252 AMEAN *03029742 SIGMA
 • 076114733102 -.268795964964E-04 -0.130772678029E-06 -0.431955709709E-04
 -0.251010716276E-07 23
 621 N 659 JE *00012373 AMEAN *01306572 SIGMA
 221 N 221 JE -.00193252 AMEAN *03029742 SIGMA
 • 077152817523 -.304548724495E-04 -0.8465158711023E-07 -0.492155122474E-04
 • 964116941603E-08 24
 601 N 661 JE *00025035 AMEAN *01725350 SIGMA
 230 N 234 JE *00061092 AMEAN *04435176 SIGMA
 • 078161030693 -.305443726102E-04 -0.9823968004887E-07 -0.430857029728E-04

-0.236392904457E-07 *07800380 25
 629 N 680 JE .00038010 AMEAN *01526576 SIGMA
 205 N 205 JE -.00180265 AMEAN *0469303 SIGMA
 *079444944914 -.316569706641E-04 -.724893923213E-07 -.489495564298E-04
 *75965530984E-08 .07875000 26
 570 N 598 JE .00050791 AMEAN *01426663 SIGMA
 176 N 176 JE *.00153381 AMEAN *03852541 SIGMA
 *080349887916 -.334878249907E-04 *.204264573137E-07 -.407949688835E-04
 *227369269087E-08 .07953300 27

STATION C 00HR GMT SEASONS COMBINED
 241 N 278 JE *.00067565 AMEAN *01919266 SIGMA
 105 N 106 JE *.00147431 AMEAN *05060921 SIGMA
 *074042283265 -.277239381306E-04 -.172601591504E-06 -.469218243608E-04
 *1780779666485E-08 .07494500 1
 542 N 602 JE *.00022881 AMEAN *01577089 SIGMA
 209 N 212 JE *.00164772 AMEAN *04477083 SIGMA
 *075196358816 -.279315360067E-04 -.159439236787E-06 -.449826084179E-04
 *829075927716E-08 .07570900 2
 661 N 698 JE *.00009230 AMEAN *01496071 SIGMA
 232 N 234 JE *.00035377 AMEAN *03241584 SIGMA
 *075987225441 -.296563753482E-04 *.970172631318E-07 -.456377518538E-04
 *671588990091E-08 *.07647400 3
 584 N 624 JE *.00000424 AMEAN *01648565 SIGMA
 181 N 189 JE *.00166467 AMEAN *05331415 SIGMA
 *077080062204 -.301489912137E-04 *.947070406343E-07 -.4666026949549E-04
 *542557404957E-08 .07723900 4
 641 N 687 JE *.00016445 AMEAN *01603484 SIGMA
 212 N 215 JE *.00161841 AMEAN *0466199 SIGMA
 *078104612716 -.315760618925E-04 *.528216917681E-07 -.466756313567E-04
 *391024612570E-08 .07800300 5
 618 N 679 JE *.00032284 AMEAN *01522870 SIGMA
 230 N 239 JE *.00120659 AMEAN *04240741 SIGMA
 *078587864990 -.316645158143E-04 *.559654636406E-07 -.478266143359E-04
 *163746659631E-08 .07876800 5
 511 N 579 JE *.00047043 AMEAN *01817861 SIGMA

178 N 187 JE -0.0165116 AMEAN * 04670829 SIGMA
 * 080096709270 -.327360963074E-04 -0.499008186073E-07 -0.487423622906E-04
 * 453386587395E-08 .07953300 7
 567 N 603 JE .00062077 AMEAN * 01537770 SIGMA
 199 N 201 JE -.00270583 AMEAN * 04060611 SIGMA
 * 080922322601 -.330978026930E-04 -.385322167389E-07 -.521727888000E-04
 * 191537477898E-07 .06030000 8

STATION C 12HR FCUR SEASONS

WINTER		SPRING		SUMMER		AUTUMN		
80 N	82 JE	95 JE	00134301 AMEAN	00134504 SIGMA	180 N	181 JE	00095520 AMEAN	00706741 SIGMA
30 N	30 JE	16 JE	000642813504E-06	-.356642813504E-06	-073710630266 -.226346300466E-04	-07494500 1	-.3666736136159E-06	-.3666736136159E-06
86 N	95 JE	16 JE	00035411 AMEAN	01629710 SIGMA	201 N	202 JE	000677772 AMEAN	02167341 SIGMA
89			-.255896664690E-04	-.261199629377E-06	* 075313248159	-.276656601003E-04	* 497229030730E-07	* 497229030730E-07
435 N	491 JE	491 JE	00025563 AMEAN	01800248 SIGMA	205 N	206 JE	00067104 AMEAN	04074660 SIGMA
180 N	181 JE	181 JE	-.193180943720E-06	-.470060522977E-04	* 076252243737	-.276656601003E-04	* 344016191205E-09	* 344016191205E-09
555 N	610 JE	610 JE	00021973 AMEAN	01606956 SIGMA	208 N	209 JE	00190853 AMEAN	04170678 SIGMA
201 N	202 JE	202 JE	-.117588015280E-06	-.488684597396E-04	* 076997308009	-.296754468676E-04	* 107464264562E-07	* 107464264562E-07
505 N	557 JE	557 JE	00003111 AMEAN	02221290 SIGMA	198 N	202 JE	00062715 AMEAN	04964564 SIGMA
171 N	181 JE	181 JE	-.00102617 AMEAN	04403168 SIGMA	* 078127126125	-.300672933888E-04	* 624477074892E-06	* 624477074892E-06
524 N	581 JE	581 JE	00016652 AMEAN	01824568 SIGMA	172 N	182 JE	00062715 AMEAN	04964564 SIGMA
359767448199E-08	-.304322137129E-04	-.108817682351E-06	-.498529138647E-04	6	6	6	6	

509 N	57 ^c	JE	.00023797	AMEAN	.01825127 SIGMA
198 N	201	JE	-.00193491	AMEAN	.04040826 SIGMA
*0800266425065	-.314015657669E-04			-.9222250506066E-07	-.506177813169E-04
*158253550920E-07	.07953300	7			
462 N	507	JE	.00044219	AMEAN	.01565672 SIGMA
188 N	193	JE	-.00514461	AMEAN	.04184472 SIGMA
*001564556731	-.345650743608E-04			-.522693523030E-08	-.546969520737E-04
*348177951990E-07	.08030000	8			
246 N	300	JE	.00054457	AMEAN	.02000630 SIGMA
102 N	103	JE	.00002256	AMEAN	.04103130 SIGMA
*082406667024	-.332052043176E-04			-.646419583941E-07	-.495401021245E-04
*990922803992E-08	.08106200	9			
 SPRING					
201 N	318	JE	.00021295	AMEAN	.01312645 SIGMA
100 N	101	JE	-.00399661	AMEAN	.02088628 SIGMA
*076139446930	-.290719417376E-04			-.135193930588E-06	-.466510085360E-04
*177910747601E-07	.07647400	10			
466 N	512	JE	-.00007597	AMEAN	.01625396 SIGMA
215 N	215	JE	.00030544	AMEAN	.03645622 SIGMA
*076796243733	-.303097511508E-04			-.907620504837E-07	-.476745753409E-04
*303262609850E-06	.07723900	11			
432 N	465	JE	.00070738	AMEAN	.01670197 SIGMA
172 N	173	JE	-.00307566	AMEAN	.03916070 SIGMA
*077609601382	-.303358690007E-04			-.921737088672E-07	-.500346686987E-04
*169009320774E-07	.07800300	12			
587 N	614	JE	.00045419	AMEAN	.01463366 SIGMA
201 N	202	JE	-.00182689	AMEAN	.03157577 SIGMA
*078603975761	-.317247663821E-04			-.585981686039E-07	-.507525503432E-04
*180347218276E-07	.07876800	13			
539 N	569	JE	.00051507	AMEAN	.01421517 SIGMA
223 N	223	JE	-.00287111	AMEAN	.03516092 SIGMA
*080244267087	-.330443121277E-04			-.370242567290E-07	-.515777649597E-04
*210546766941E-07	.07953300	14			
375 N	423	JE	.00079344	AMEAN	.01703104 SIGMA
178 N	178	JE	.00061106	AMEAN	.02692804 SIGMA

* 080623726684 -0 326331959913E-04 -0 538423372070E-07 -.493483936595E-04
• 939045747715E-06 * 38030000 15

SUMMER
355 N 373 JE -.00004078 AMEAN .01342009 SIGMA
133 N 133 JE -.00132252 AMEAN .03320106 SIGMA
• 075130339656 -.29013303429E-04 -.112139295423E-06 -.452178922265E-04
-.769563306559E-08 .07570900 16
595 N 60 JE -.00005210 AMEAN .01126172 SIGMA
246 N 247 JE -.00037549 AMEAN .03526676 SIGMA
• 076092496624 -.304555925747E-04 -.796356968813E-07 -.452472088419E-04
-.105488633346E-07 .87647400 17
526 N 556 JE -.00012696 AMEAN .011330268 SIGMA
208 N 208 JE *.00074210 AMEAN .03680023 SIGMA
• 076796692980 -.314243847545E-04 -.438332611923E-07 -.427053419662E-04
-.33541697701E-07 .07723900 18
593 N 615 JE *.00018075 AMEAN .01192169 SIGMA
214 N 217 JE -.00254871 AMEAN .03748987 SIGMA
• 0708246874917 -.321760576239E-04 -.333785297614E-07 -.470653046258E-04
-.259236554952E-08 .07800400 19
326 N 352 JE *.00209961 AMEAN .01280475 SIGMA
150 N 150 JE -.00024834 AMEAN .02087523 SIGMA
• 077039369956 -.323533648650E-04 -.235594993941E-07 -.4503280023136E-04
-.180776775489E-07 .07876800 20

FALL
91 N 95 JE *.00023884 AMEAN .01072141 SIGMA
8 N 8 JE -.00057191 AMEAN .03699301 SIGMA
• 074622179924 -.285946341695E-04 -.134221747253E-06 -.526137260767E-04
• 339944692122E-07 .07494500 21
240 N 254 JE *.00009585 AMEAN .01303679 SIGMA
80 N 81 JE -.00157849 AMEAN .03842507 SIGMA
• 075341095531 -.282316684595E-04 -.14837222206E-06 -.470050503915E-04
• 1226729991922E-07 .07570900 22
689 N 667 JE *.00011848 AMEAN .01724950 SIGMA
253 N 253 JE *.000082682 AMEAN .03643744 SIGMA

• 076114410248 - 0296093170327E-04 - 0103369417468E-06 - 0472212404955E-04
 - 0452156102704E-09 .07647400 23
 641 N 693 JE - 00016662 AMEAN • 01576146 SIGMA
 234 N 246 JE - 00102243 AMEAN • 05140103 SIGMA
 • 077254026385 -.301630756097E-04 - 0.996926963734E-07 - 0.445653 '64658E-04
 - 0164632400067E-07 .07723900 24
 585 N 632 JE • 00025951 AMEAN • 01500314 SIGMA
 215 N 220 JE - 00346073 AMEAN • 04574497 SIGMA
 • 078267436987 -.310176646715E-04 - 0.784668460403E-07 - 0.488185339044E-04
 • 982118832189E-06 .07800300 25
 598 N 625 JE • 00056807 AMEAN • 01390782 SIGMA
 234 N 237 JE - 00151375 AMEAN • 04656462 SIGMA
 • 079354746731 -.326738597128E-04 - 0.385244129582E-07 - 0.471460913078E-04
 - 0.637494363270E-08 .07876800 26
 493 N 562 JE • 00053616 AMEAN • 013907016 SIGMA
 193 N 194 JE - 00271715 AMEAN • 04464628 SIGMA
 • 080606464931 -.335045549947E-04 - 0.299049815553E-07 - 0.507972961023E-04
 • 1500010379997E-07 .07953300 27

STATION C 12HR SEAPONS COMBINED
 163 N 185 JE • 00071632 AMEAN • 01990139 SIGMA
 39 N 43 JE • 00205894 AMEAN • 06377341 SIGMA
 • 074132127585 -.261809486929E-04 - 0.217797523168E-06 - 0.453675600083E-04
 - 0450423081798E-08 .07494500 1
 507 N 540 JE - 00013041 AMEAN • 01514052 SIGMA
 166 N 172 JE - 00182289 AMEAN • 04653447 SIGMA
 • 075358915305 -.284656154898E-04 - 0.1390666016458E-06 - 0.462685745843E-04
 - 0.645572242094E-09 .07570900 2
 507 N 624 JE • 00020079 AMEAN • 01661910 SIGMA
 225 N 233 JE - 00203609 AMEAN • 04869516 SIGMA
 • 076271591386 -.305163898072E-04 - 0.754774796930E-07 - 0.459876125065E-04
 - 0.911324646356E-08 .07647400 3
 540 N 564 JE - 00005009 AMEAN • 01371726 SIGMA
 193 N 199 JE - 00019837 AMEAN • 04790721 SIGMA
 • 076979459084 -.308788279965E-04 - 0.673526331249E-07 - 0.427948518739E-04
 - 0.328083986666E-07 .07723900 4

TR 82-81

916 N	536 JE	- .00013569	AMEAN	* .01543790 SIGMA
183 N	187 JE	- .00199122	AMEAN	* .04531566 SIGMA
* 077406620038	- .300534920123E-04	- .676901069213E-07	- .473520275576E-04	
* 1040289003355E-09	.07000300	5		
586 N	620 JE	* .00035943	AMEAN	* .01491915 SIGMA
226 N	226 JE	- * .00116632	AMEAN	* .04044945 SIGMA
* 079059615607	- .320533910711E-04	- .586325706766E-07	- .484418142961E-04	
* 421052420233E-08	.07876600	6		
538 N	589 JE	* .00043485	AMEAN	* .01567976 SIGMA
225 N	226 JE	- * .00274972	AMEAN	* .03937568 SIGMA
* 080502865266	- .3360623853A5E-04	- .2964600825201E-07	- .512731E20622E-04	
* 164357501503E-07	.07953300	7		
560 N	589 JE	* .00086630	AMEAN	* .01236586 SIGMA
260 N	260 JE	- * .00322612	AMEAN	* .03194724 SIGMA
* 081189039600	- .344179522903E-04	- .163738061022E-06	- .540332986874E-04	
* 30866457900E-07	.08030J00	8		
299 N	342 JE	* .00043411	AMEAN	* .01069886 SIGMA
100 N	102 JE	- * .00096213	AMEAN	* .04136389 SIGMA
* 082547643058	- .339103645200E-04	- .422930034466E-07	- .513051322245E-04	
* 109100076961E-07	.06106200	9		

TR 82-81

APPENDIX D

DENSITY RATIO PROFILES FROM STATION E

TR 82-81

DENSITY RATIO PROFILES FOR STATION E

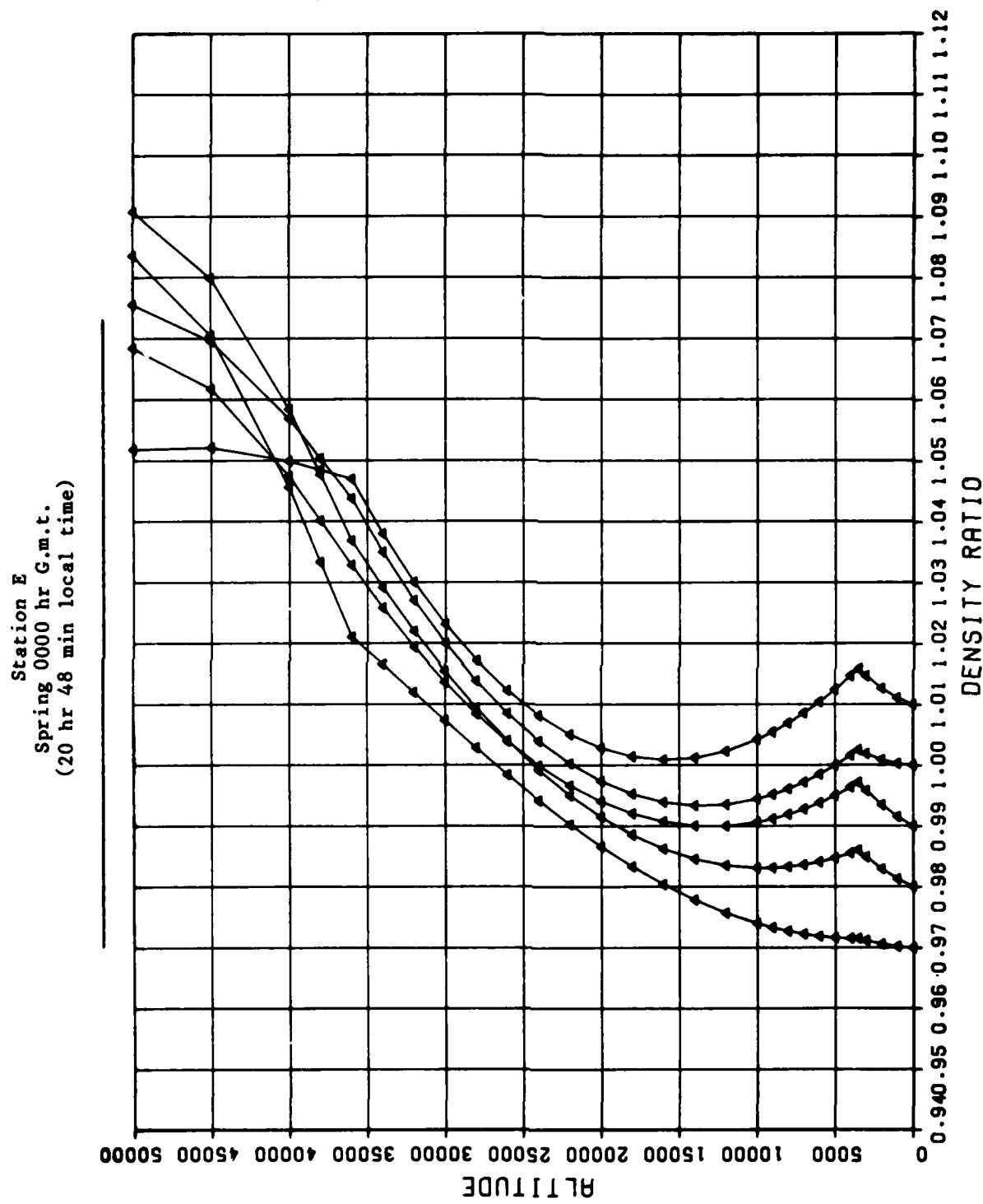
Station E is in the mid-Atlantic east of Bermuda. The uniformity and the shape of the density profiles indicate that the U.S. Standard atmosphere does not represent the atmosphere over station E too well for the period sampled. Almost all the curves above 3,500 ft are fishhook shaped. Below 3,500 ft, the density ratios increase with altitude. The lapse rate is larger than standard, which is referred to in meteorology as a "superadiabat." From 3,500 to 35,000 ft, the density ratio curves are all concave, as seen from the right. That is, density to about 15,000 ft decreases with altitude more than in the standard atmosphere. Above 15,000 ft, the density ratios increase with altitude. Density ratios are all greater than one above 30,000 ft, and they grow larger, regardless of surface density ratios. Overall, when density is two percent below standard at the surface, it averages three percent above standard at 35,000 ft. Above 35,000 ft, the curves are more erratic, which is probably due to the higher noise level in the observations.

Some seasonal differences are apparent in this region. For example, in summer, both at 2100 hr and 0900 hr local time, the density ratios increase linearly from 35,000 to 45,000 ft to a value of 11 percent above standard. This seasonal behavior may be associated with the seasonal change in the height and temperature of the tropopause.

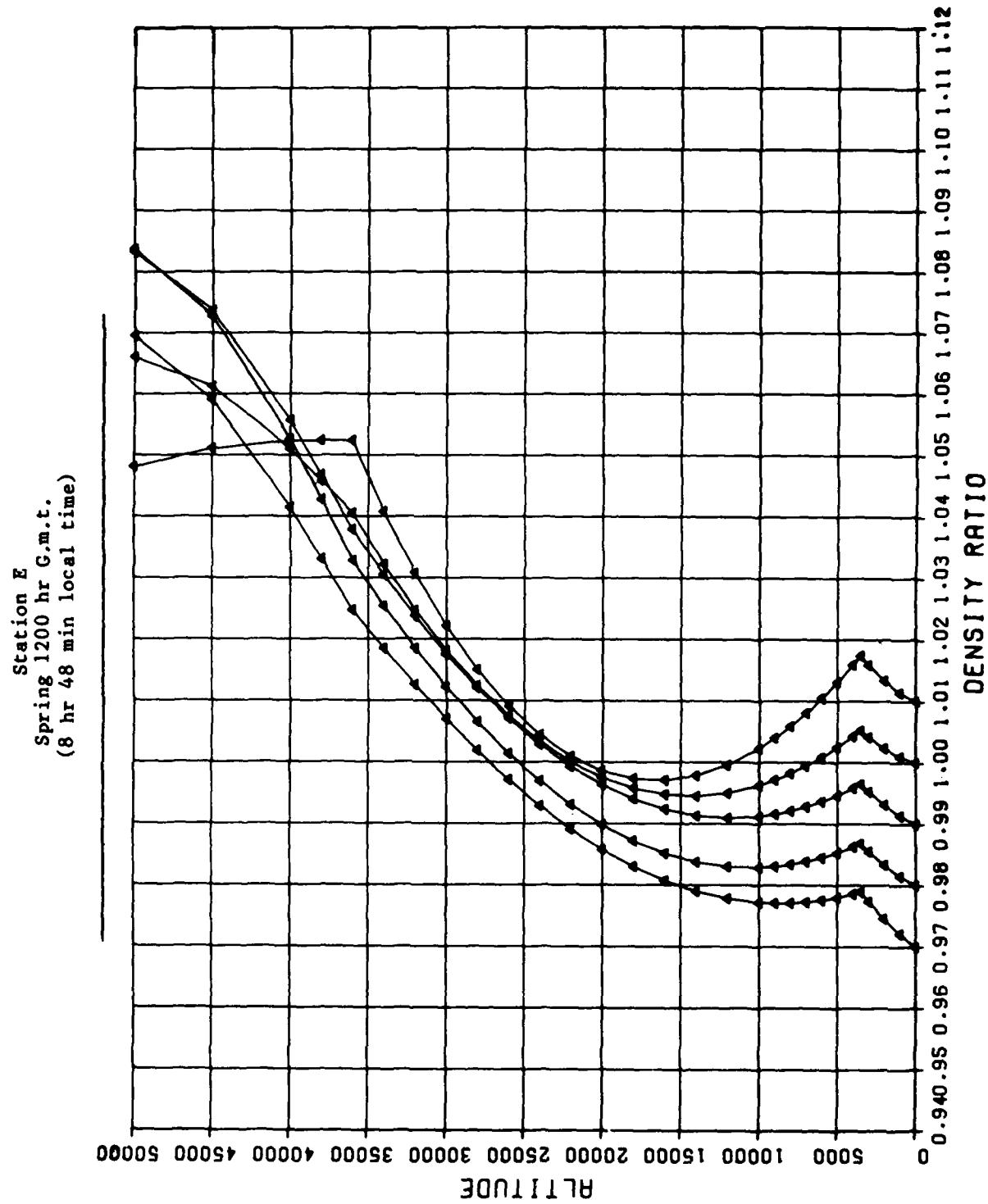
The diurnal differences are very small. When the 9 a.m. and 9 p.m. curves are superimposed, the coincidence of the curves is remarkable. This could mean that there are no diurnal changes in density; or that, as the surface temperature and density change diurnally, the density aloft changes in a corresponding manner, and the correlation is preserved. It could also be due to the fact that 9 a.m. and 9 p.m. temperatures are nearly the same. At stations N and V, the sonde times would likely correspond to greater differences in surface temperature and density.

The values for surface density reflect the seasonal changes in temperature. Surface density class medians ranged from 0.95 to 0.98 in summer; in winter, they ranged from 0.97 to 1.02.

TR 82-81

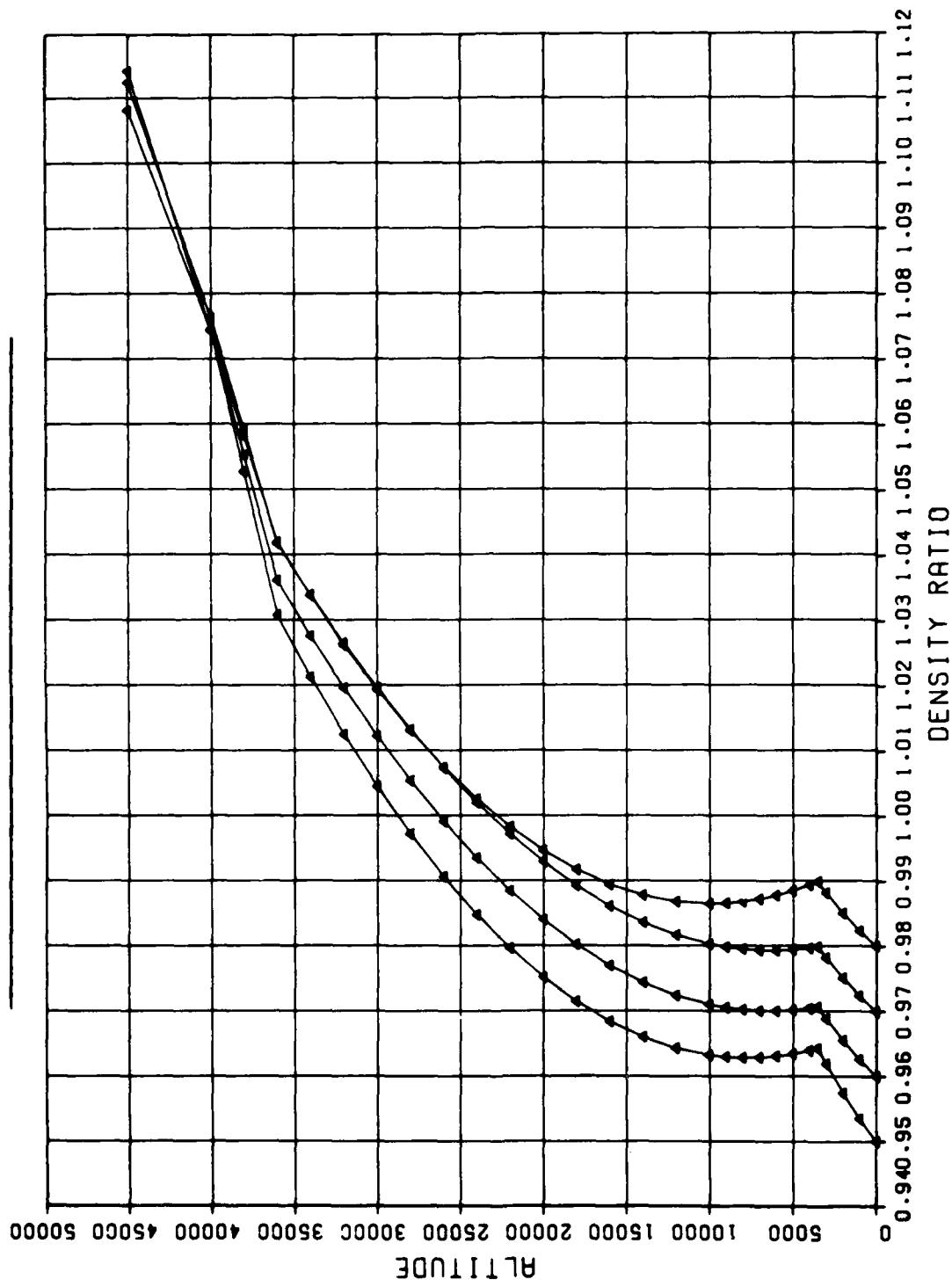


TR 82-81

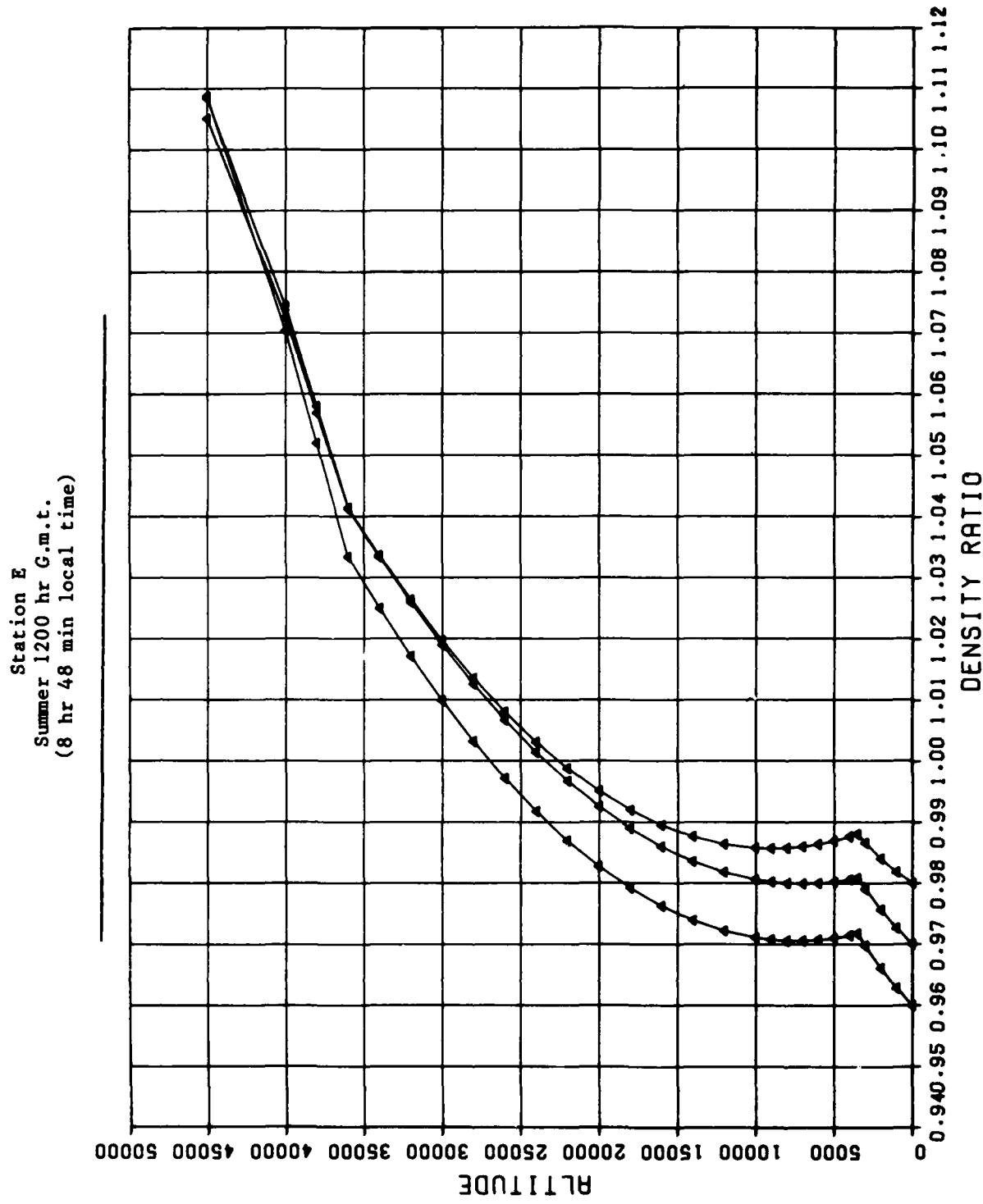


TR 82-81

Station E
Summer 0000 hr G.m.t.
(20 hr 48 min local time)

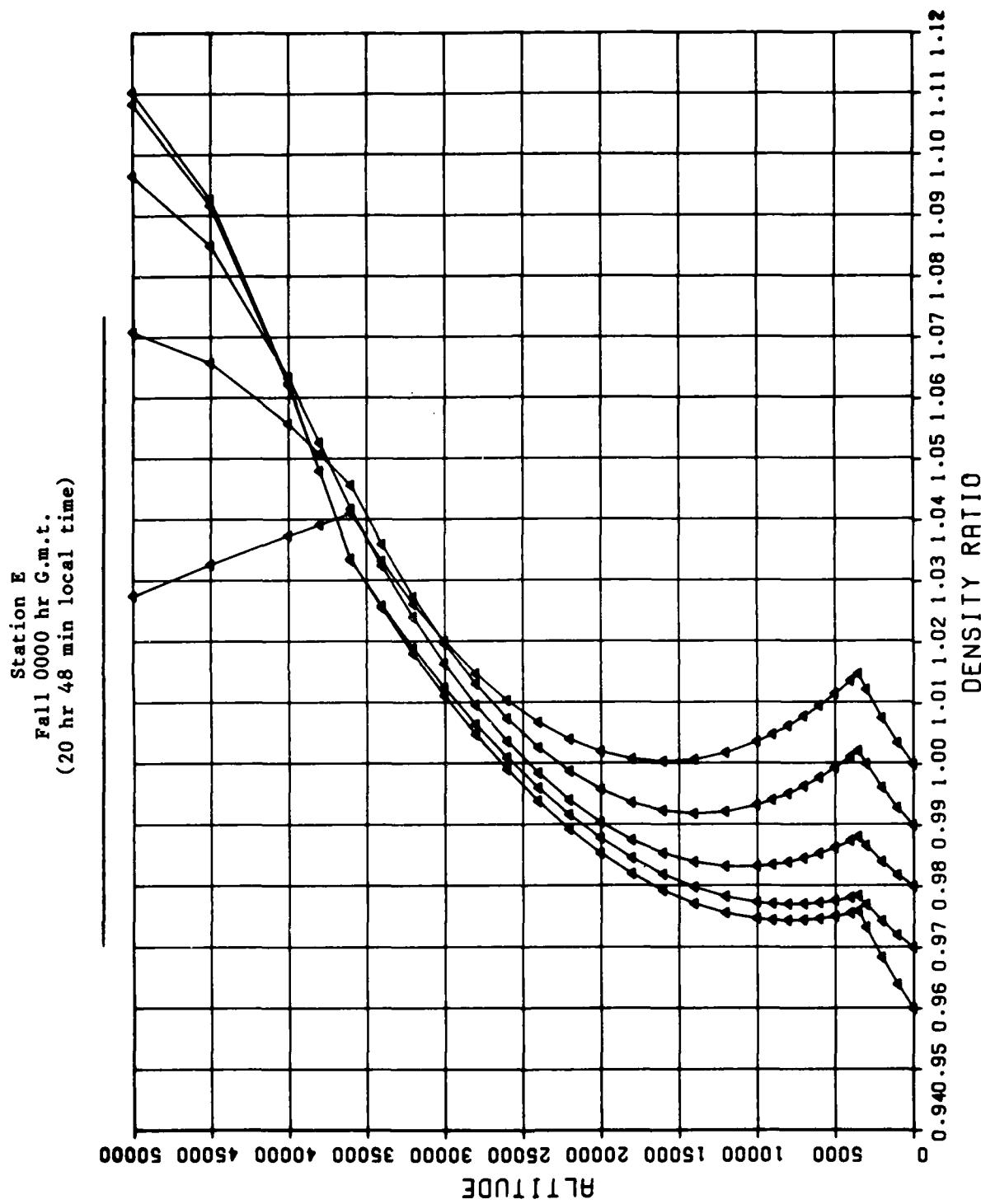


TR 82-81

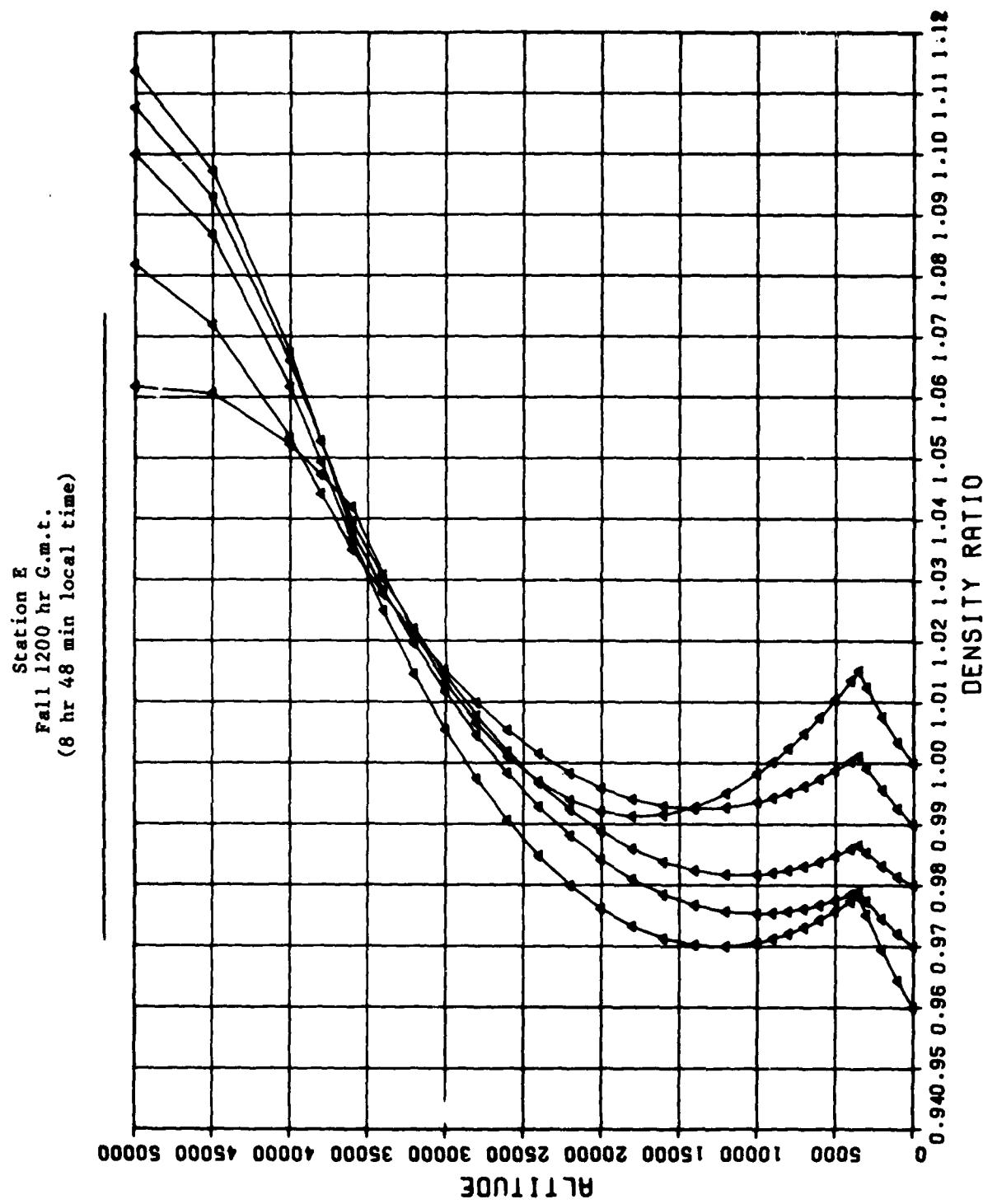


D-7

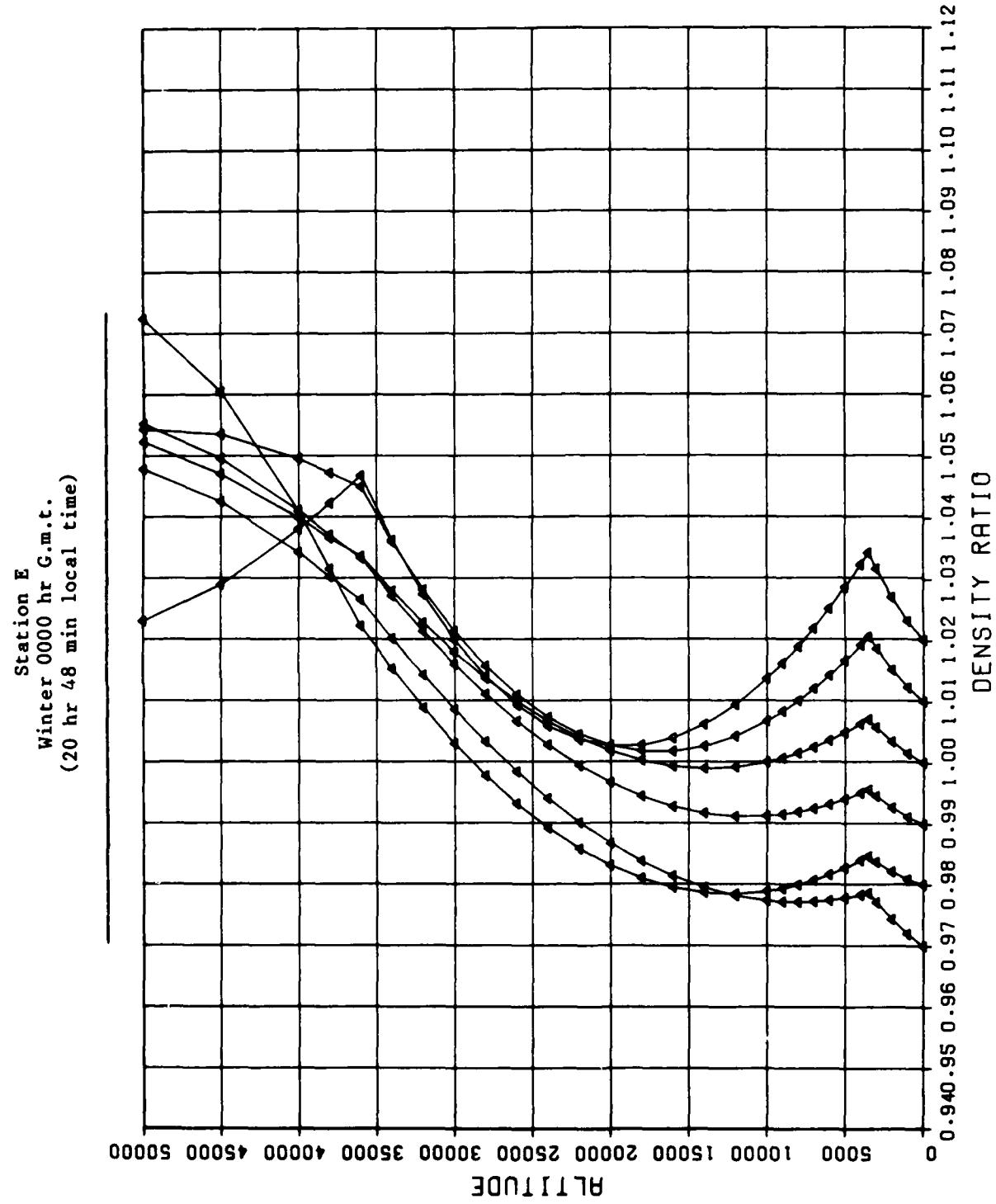
TR 82-81



TR 82-81

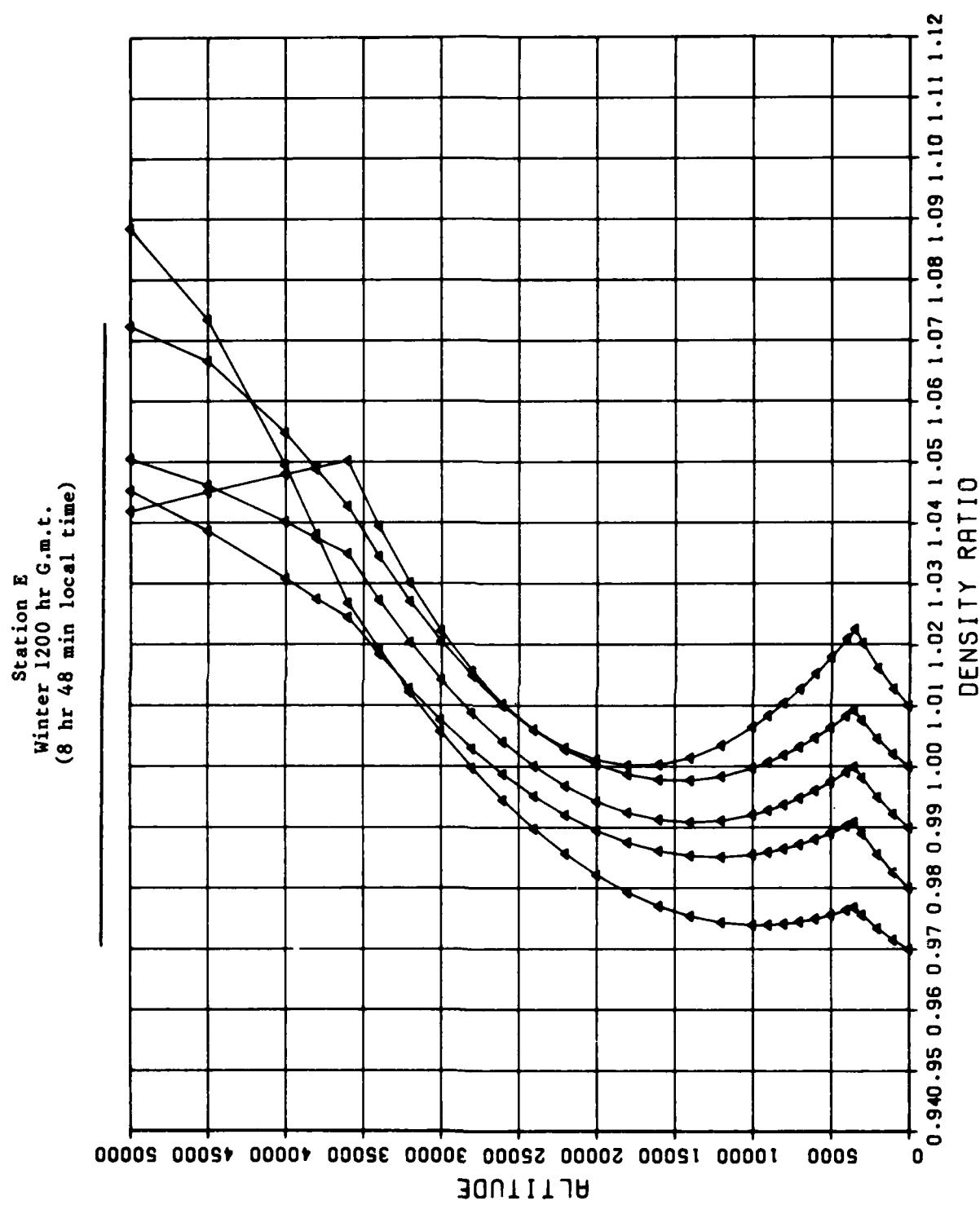


TR 82-81



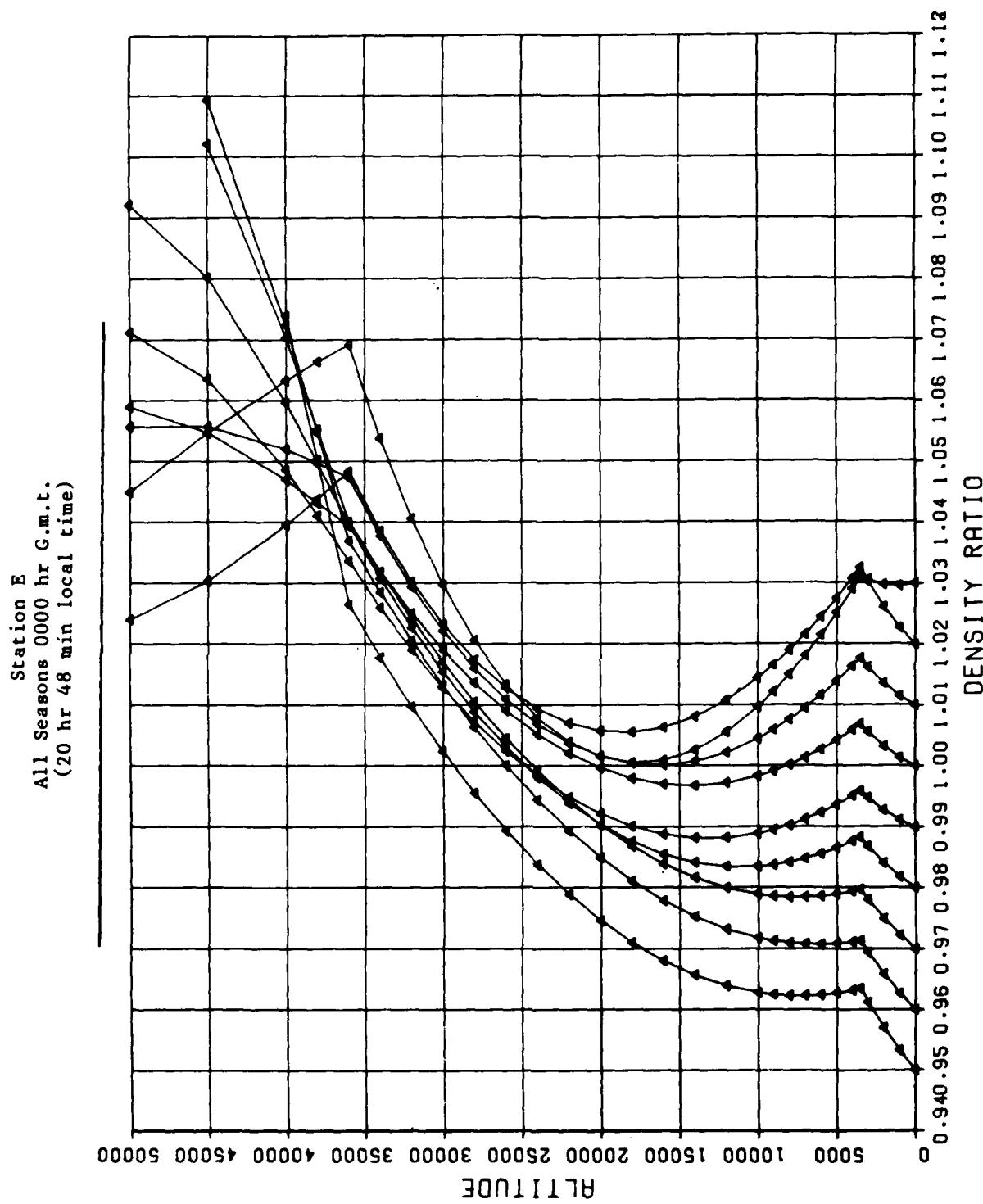
D-10

TR 82-81



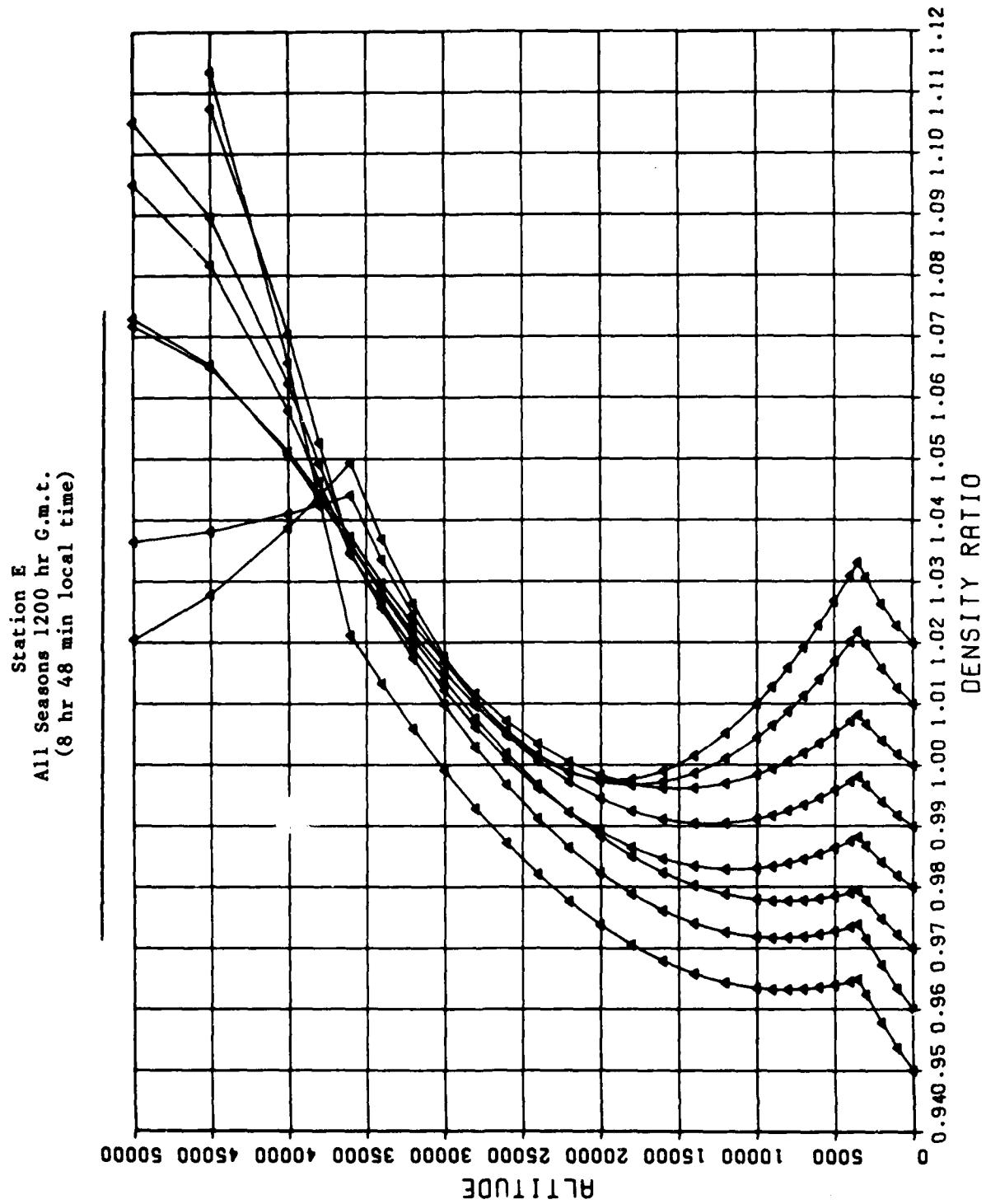
D-11

TR 82-81



D-12

TR 82-81



TR 82-81

APPENDIX E

BALLISTIC DENSITY PROFILES FOR STATION E

AD-A119 496

NAVAL SURFACE WEAPONS CENTER DAHLGREN VA
A METHOD TO CORRELATE THE UPPER AIR DENSITY WITH SURFACE DENSITY--ETC(U)

F/G 4/1

JUL 82 L J MCANELLY.
UNCLASSIFIED
NSWC/TR-82-81

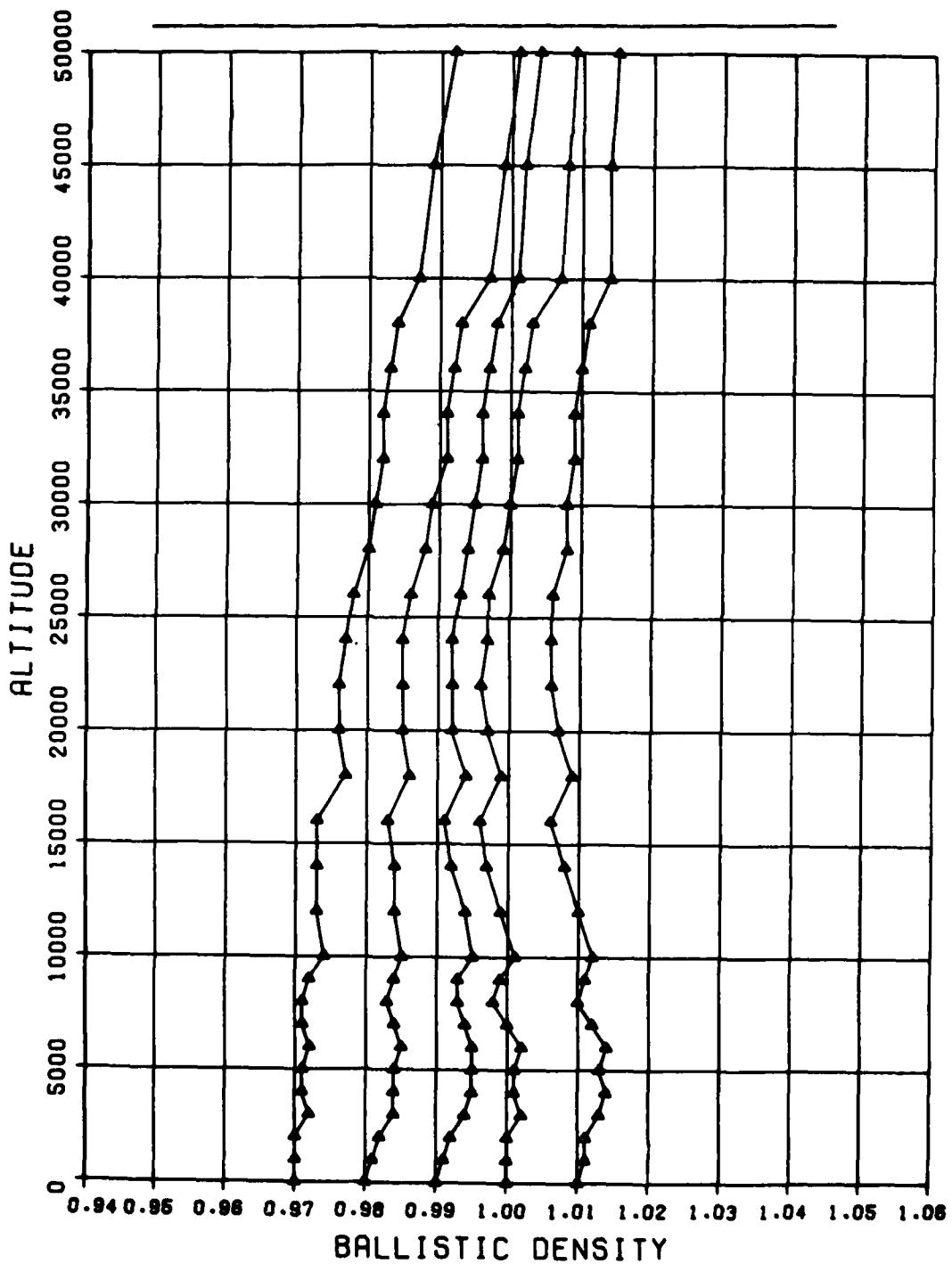
NL

2 of 2
R1
2022-4

END
DATE
FILED
11-82
DTIC

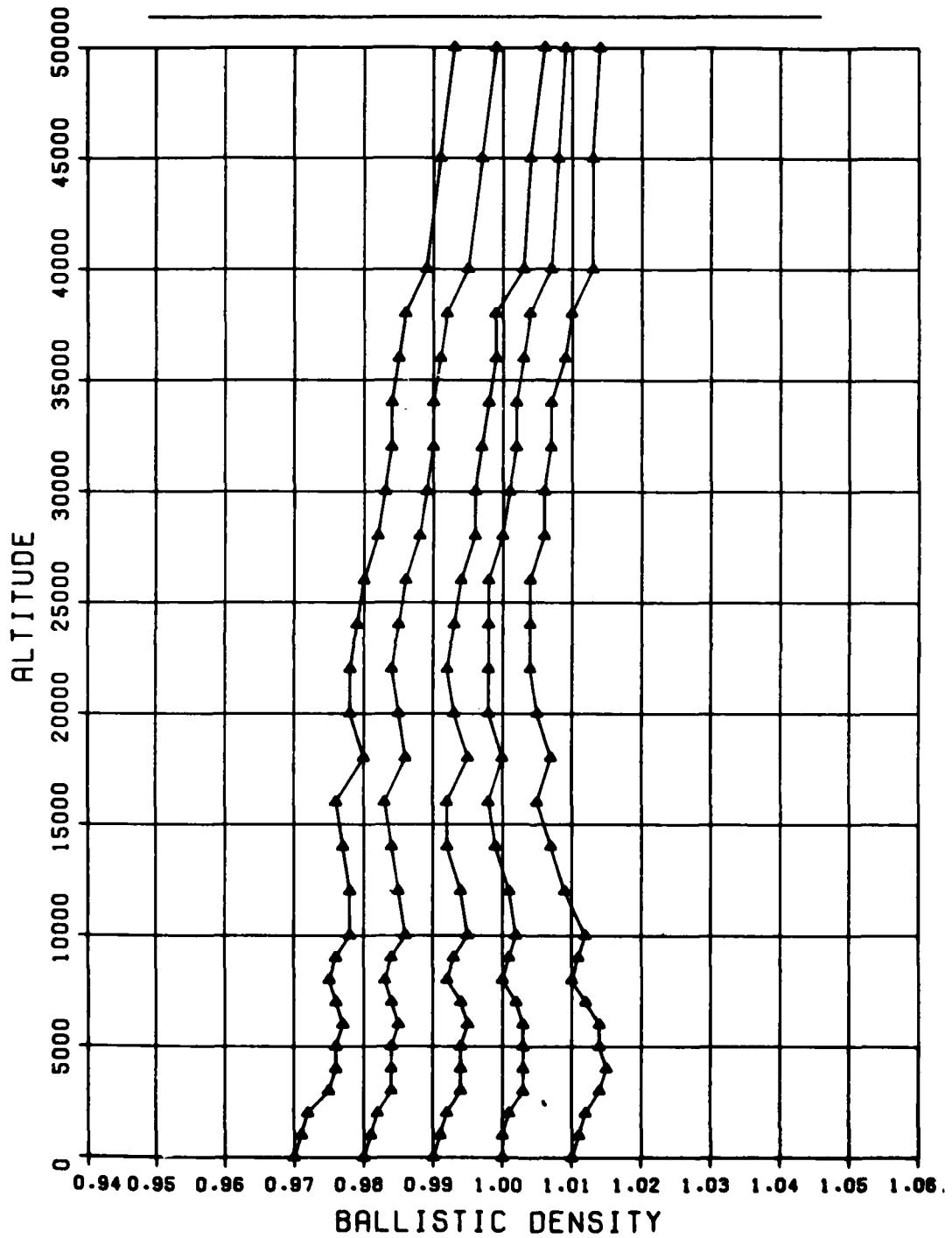
TR 82-81

Station E
Spring 0000 hr G.m.t.
(20 hr 48 min local time)



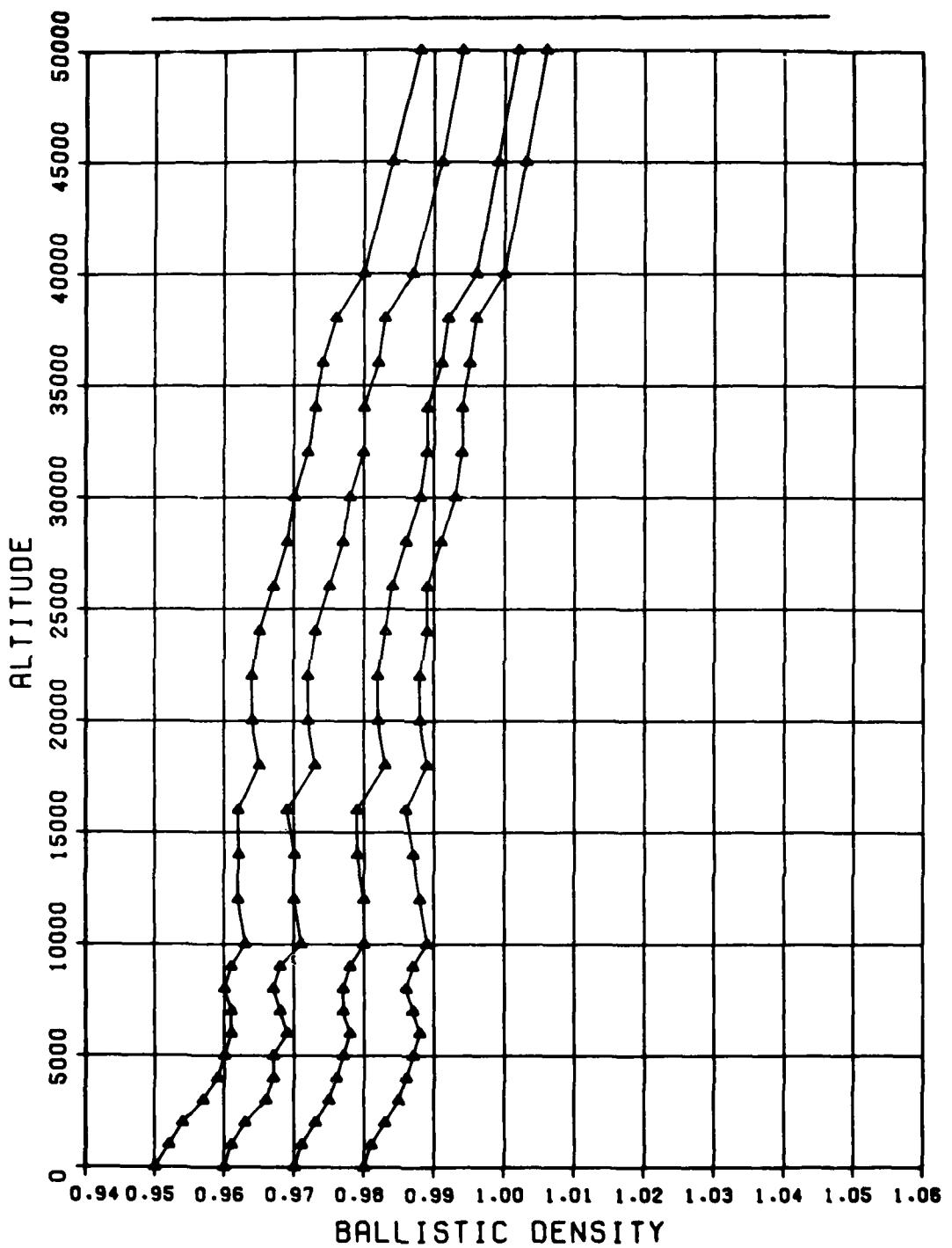
TR 82-81

Station E
Spring 1200 hr G.m.t.
(8 hr 48 min local time)



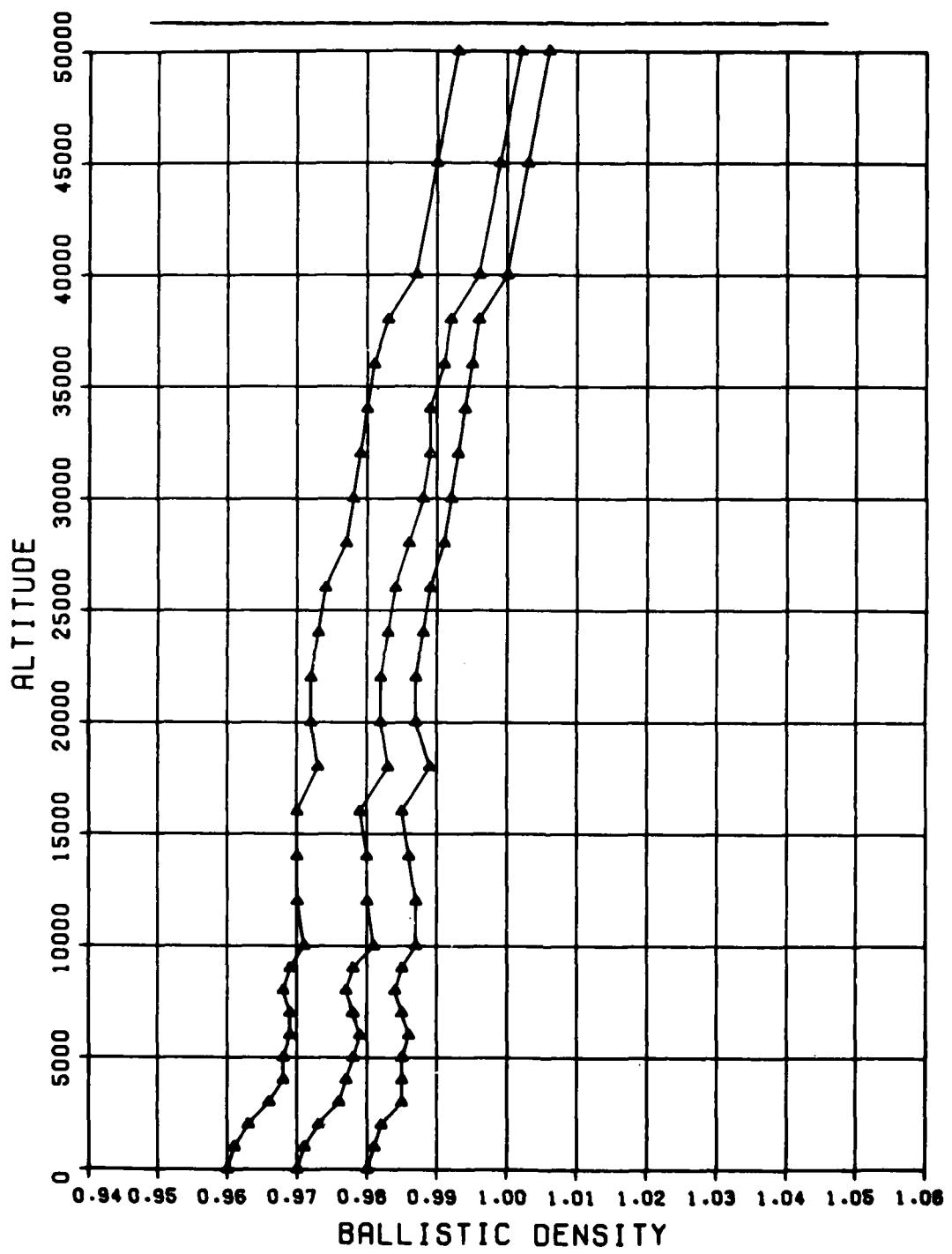
TR 82-81

Station E
Summer 0000 hr G.m.t.
(20 hr 48 min local time)



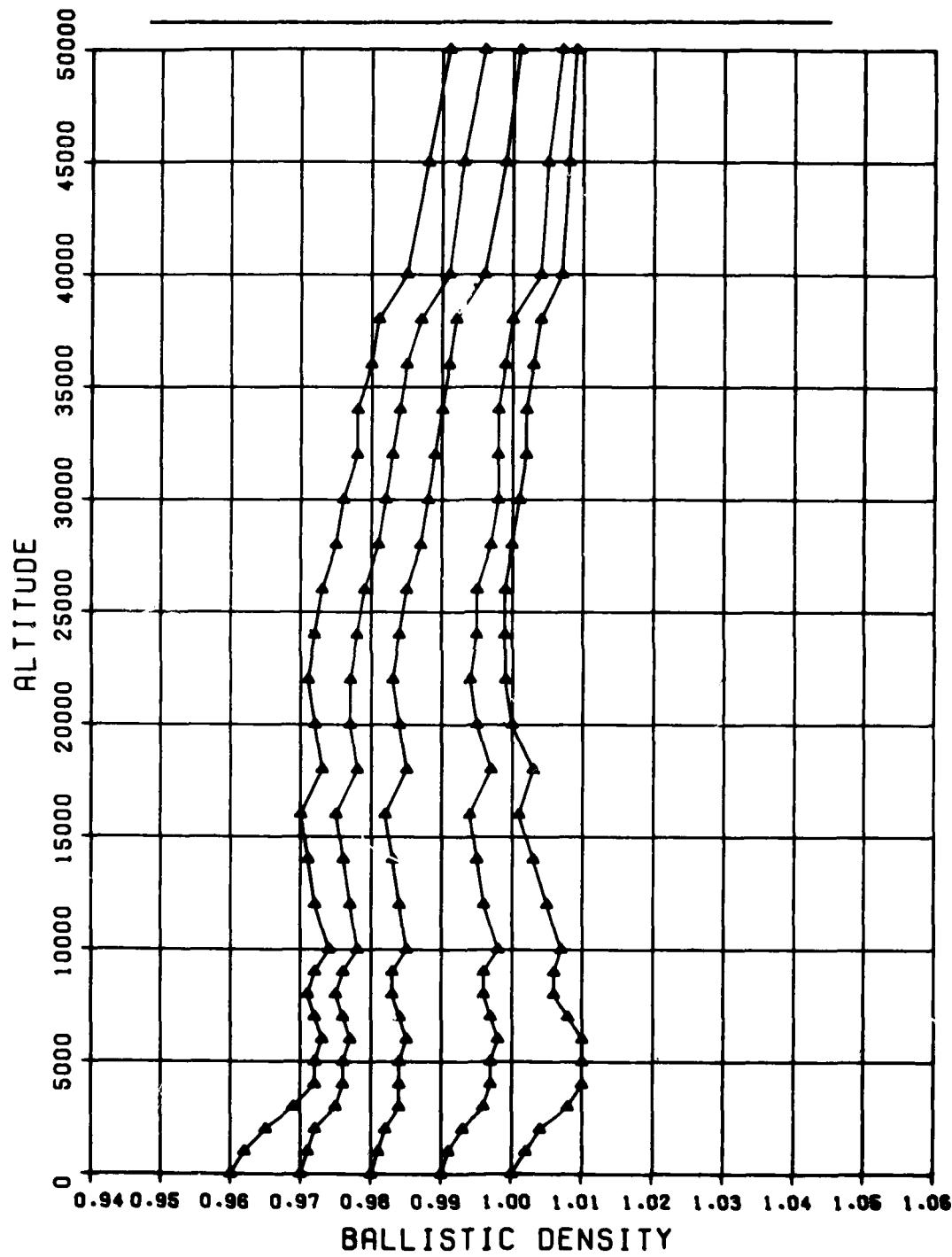
TR 82-81

Station E
Summer 1200 hr G.m.t.
(8 hr 48 min local time)



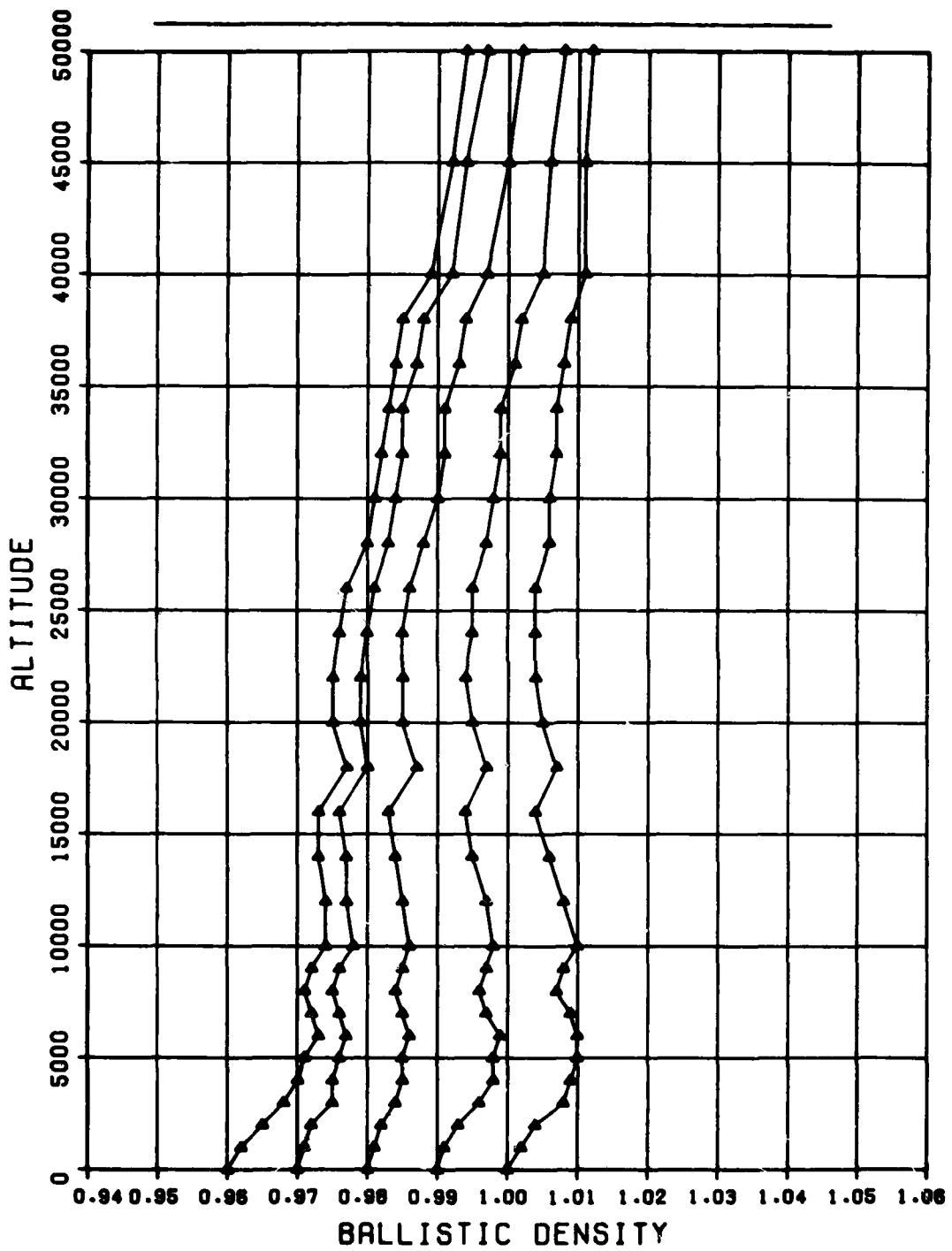
TR 82-81

Station E
Fall 0000 hr G.m.t.
(20 hr 48 min local time)



TR 82-81

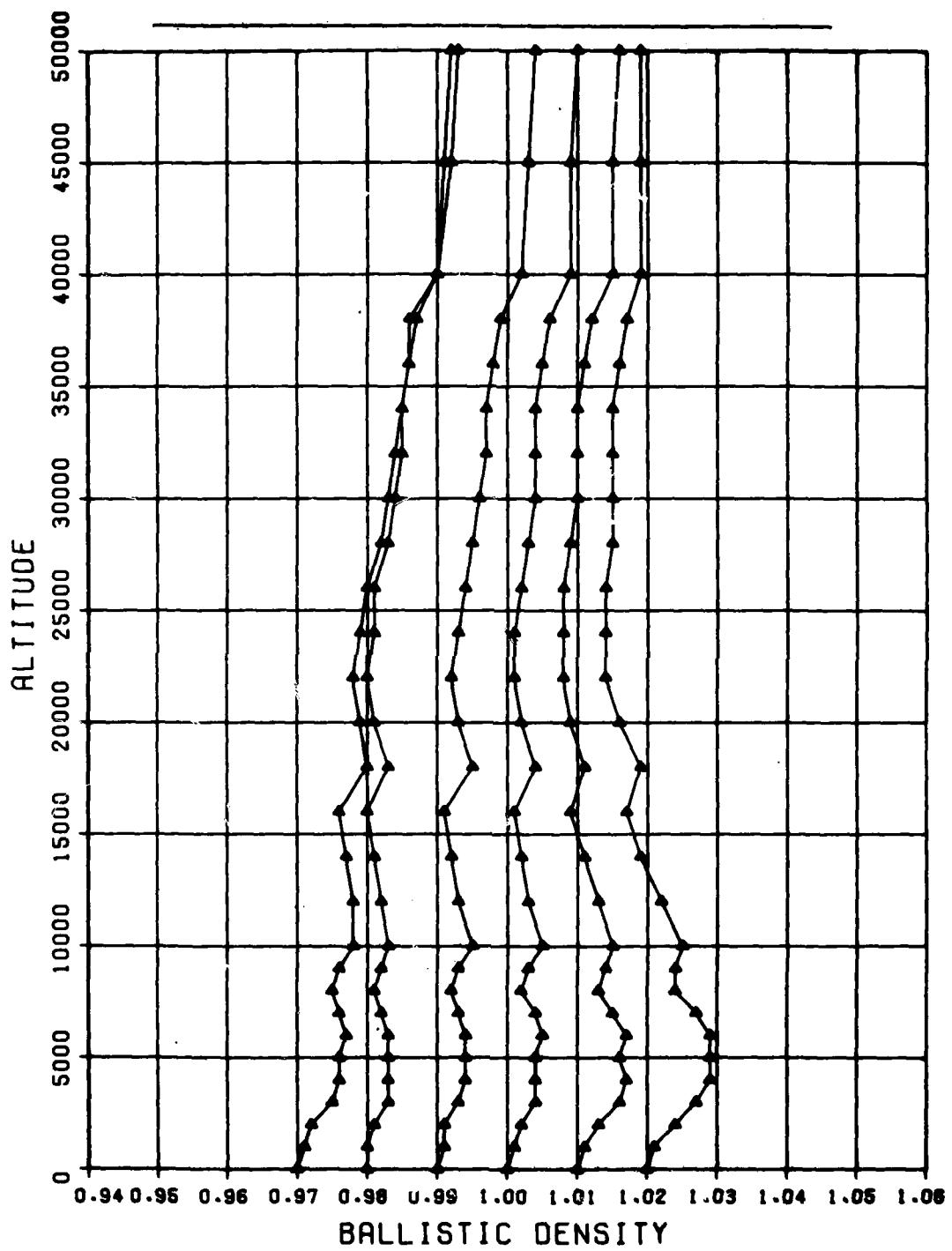
Station E
Fall 1200 hr G.m.t.
(8 hr 48 min local time)



E-8

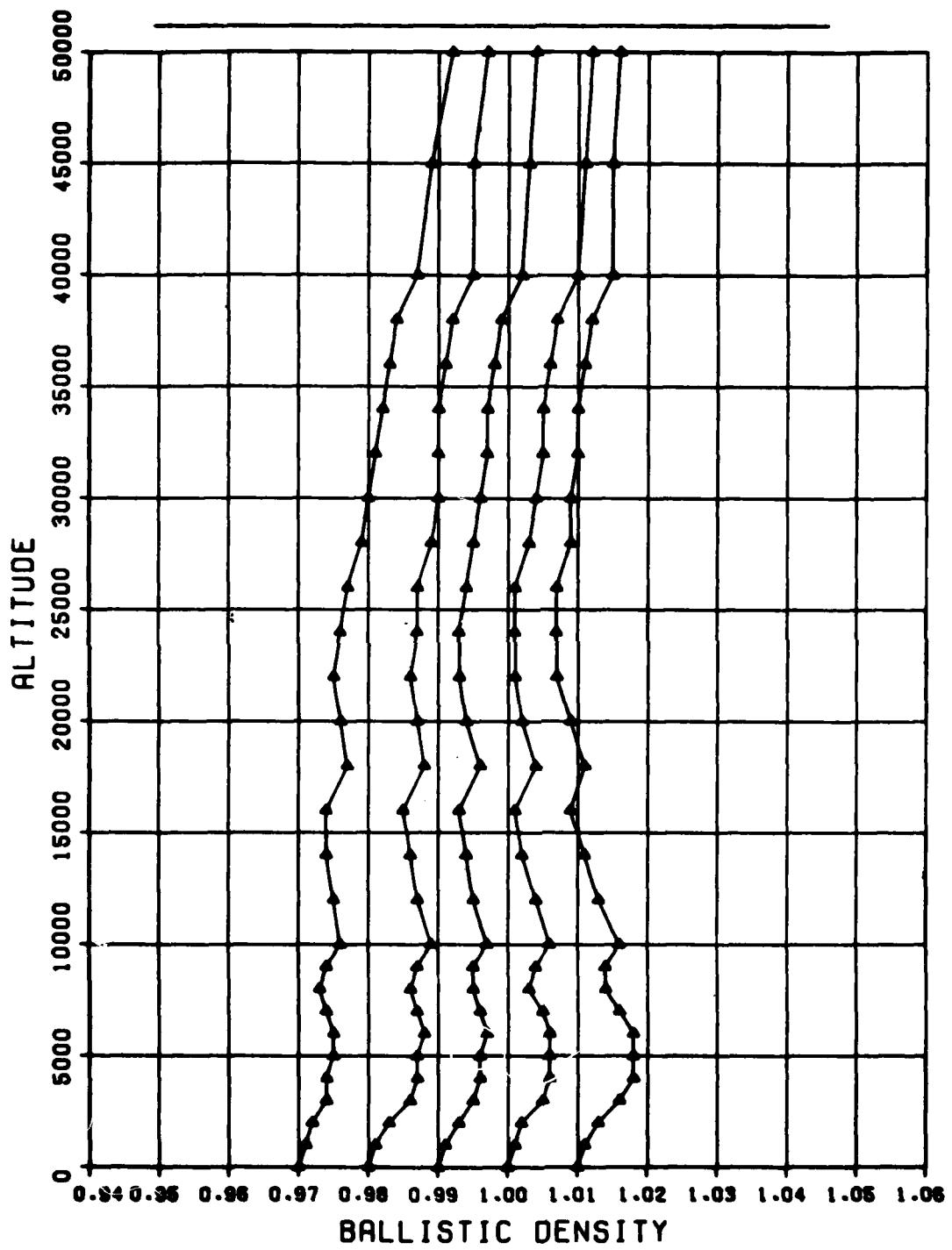
TR 82-81

Station E
Winter 0000 hr G.m.t.
(20 hr 48 min local time)



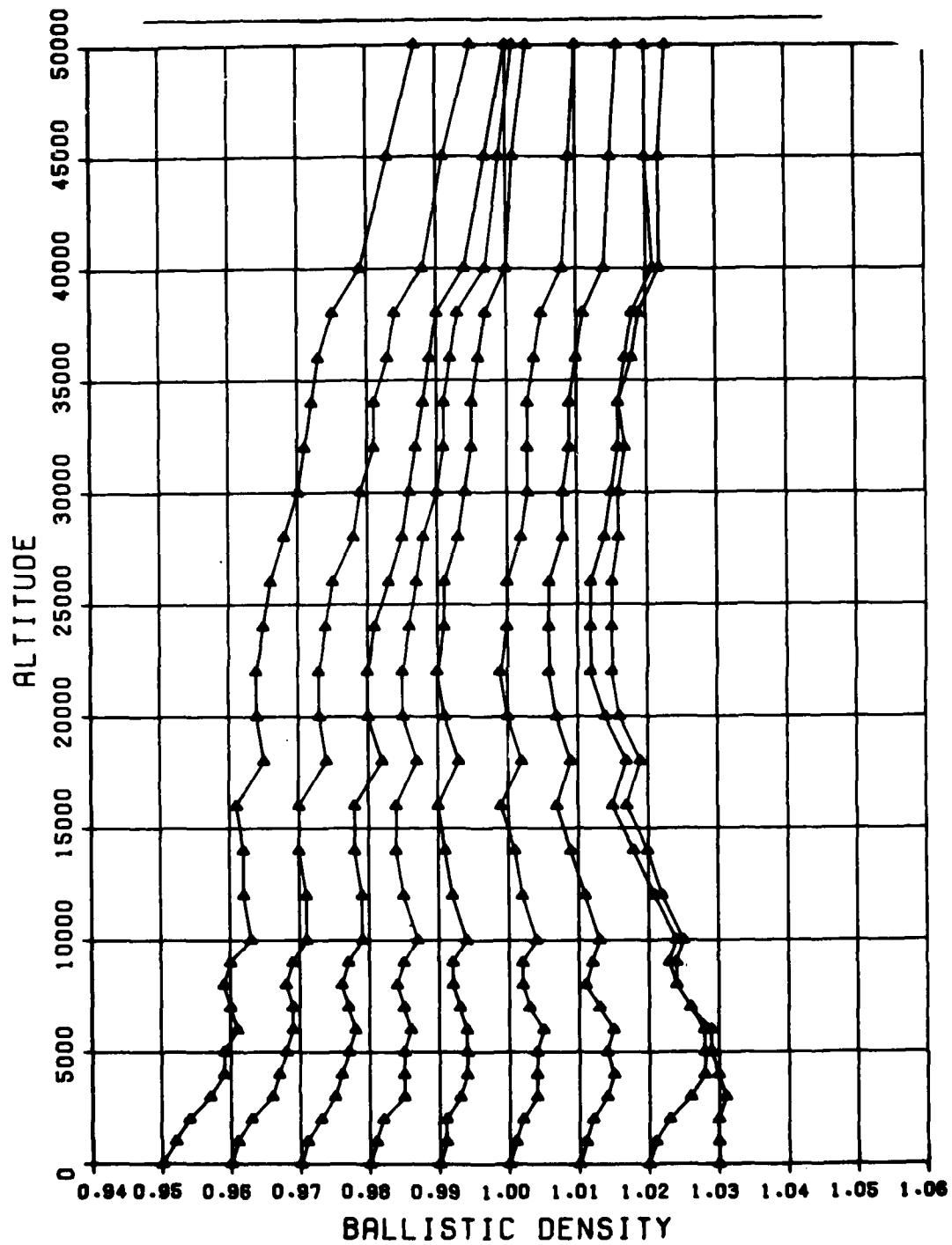
TR 82-81

Station E
Winter 1200 hr G.m.t.
(8 hr 48 min local time)



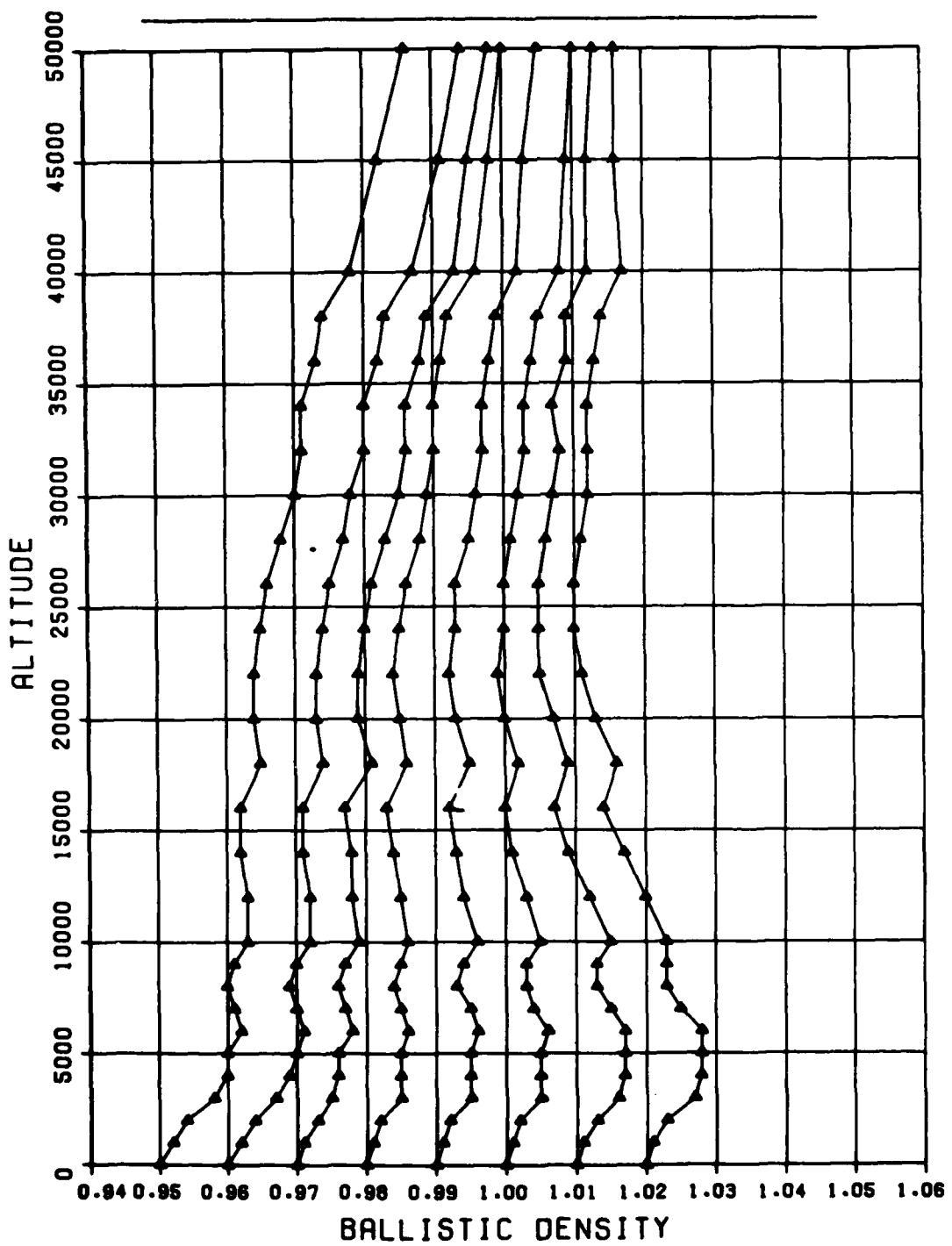
TR 82-81

Station E
All Seasons 0000 hr G.m.t.
(20 hr 48 min local time)



TR 82-81

Station E
All Seasons 1200 hr G.m.t.
(8 hr 48 min local time)



TR 82-81

APPENDIX F

SELECTED BALLISTIC DENSITIES FOR STATIONS E, N, AND C

TR 82-81

Local time corresponding to:

<u>Station</u>	<u>0000 hr G.m.t.</u>	<u>1200 hr G.m.t.</u>
E	20 hr 48 min	08 hr 48 min
V	10 hr 54 min	22 hr 54 min
C	21 hr 38 min	09 hr 38 min
D	21 hr 16 min	09 hr 16 min
N	14 hr 40 min	02 hr 20 min

(To be used with the following tables.)

BALLISTIC DENSITY

Altitude = 30,000 ft

Station	Surface Density	0000 hr G.m.t.			1200 hr G.m.t.		
		W	S	F	W	S	F
E	0.95	-	-	0.970	0.970	-	-
V	-	-	-	0.968	0.971	0.968	-
C	-	-	-	-	-	-	0.967
D	-	-	-	-	-	-	-
N	-	-	-	-	-	-	-
E	0.96	-	-	0.978	0.981	0.979	-
V	-	-	-	0.975	0.973	0.975	-
C	-	-	-	-	-	-	0.974
D	-	-	-	-	-	-	-
N	-	-	-	0.981	-	0.979	-
E	0.97	0.983	0.981	0.988	0.984	0.986	0.980
V	0.971	0.972	0.976	0.978	0.975	-	0.973
C	-	-	-	-	-	-	0.976
D	-	-	-	0.978	0.980	0.977	-
N	0.982	0.980	0.982	0.983	0.982	0.984	-
E	0.98	0.984	0.989	0.993	0.990	0.990	0.989
V	0.984	0.980	0.979	0.986	0.980	0.984	0.980
C	0.971	-	-	0.973	0.972	0.968	-
D	0.983	-	0.987	0.984	0.985	0.981	0.982
N	0.985	0.986	0.984	0.988	0.985	0.988	0.986

BALLISTIC DENSITY

Altitude = 30,000 ft

TR 82-81

Station	Surface Density	00000 hr G.m.t.			1200 hr G.m.t.						
		W	S	SU	F	A	W	S	SU	F	A
E	0.99	0.996	0.995	0.987	0.998	0.994	0.996	0.996	-	0.998	0.996
V	0.991	0.986	0.984	0.995	0.991	0.992	0.987	0.987	-	0.993	0.989
C	0.977	0.978	0.979	0.980	0.978	0.980	-	0.978	0.980	0.980	0.991
D	0.988	0.989	0.992	0.991	0.992	0.990	0.991	0.991	0.990	0.990	0.991
N	0.994	0.990	0.989	0.994	0.993	0.993	0.989	0.990	0.996	0.992	-
E	1.00	1.004	1.000	-	1.006	1.003	1.004	1.001	-	1.001	1.002
V	0.999	0.995	-	1.001	0.998	0.998	0.993	-	1.003	0.995	-
C	0.986	0.987	0.987	0.987	0.986	0.985	0.983	0.985	0.986	0.984	-
D	0.996	0.995	0.995	0.998	0.997	0.997	0.995	0.995	0.996	0.994	-
N	1.003	0.998	-	1.000	1.000	1.001	0.999	-	1.002	1.000	-
E	1.01	1.010	1.008	-	-	1.008	1.009	1.006	-	-	1.007
V	1.006	1.001	-	-	1.005	1.004	0.999	-	-	-	1.003
C	0.993	0.992	0.991	0.994	0.993	0.992	0.989	0.990	0.994	0.992	-
D	1.002	1.002	-	1.000	1.002	1.002	1.000	-	1.002	1.002	-
N	1.009	-	-	-	1.010	1.011	1.007	-	-	-	1.009
E	1.02	1.015	-	-	-	1.016	-	-	-	-	1.012
V	1.011	1.009	-	-	1.008	1.008	1.007	-	-	-	1.009
C	1.002	0.996	0.997	1.001	0.998	1.001	0.999	0.999	1.002	0.999	-
D	1.009	1.005	-	-	1.010	1.008	1.004	-	1.008	1.009	-
N	-	-	-	-	-	-	-	-	-	-	-

BALLISTIC DENSITY

Altitude = 30,000 ft

<u>Station</u>	<u>Surface Density</u>	0000 hr G.m.t.			1200 hr G.m.t.		
		W	S	F	W	S	F
E	1.03	-	-	-	-	-	-
V	-	-	-	-	-	-	-
C	1.008	1.006	0.999	1.010	1.006	1.008	-
D	1.103	1.011	-	1.012	1.013	1.013	-
N	-	-	-	-	-	-	-
E	1.04	-	-	-	-	-	-
V	-	-	-	-	-	-	-
C	1.105	1.013	-	1.014	1.012	1.015	-
D	1.020	-	-	-	1.019	1.022	-
N	-	-	-	-	-	-	-
E	1.05	-	-	-	-	-	-
V	-	-	-	-	-	-	-
C	1.024	1.018	-	-	1.021	1.019	-
D	1.028	-	-	-	1.027	1.027	-
N	-	-	-	-	-	-	-
E	1.06	-	-	-	-	-	-
V	-	-	-	-	-	-	-
C	-	-	-	-	-	-	-
D	-	-	-	-	-	-	-
N	-	-	-	-	-	-	-

BALLISTIC DENSITY

Altitude = 50,000 ft

Station	Surface Density	0000 hr G.m.t.				1200 hr G.m.t.			
		W	S	SU	F	W	S	SU	F
E	0.95	-	-	0.988	-	0.987	-	-	-
V	-	-	-	0.986	0.984	0.984	-	-	0.986
C	-	-	-	-	-	-	-	-	0.982
D	-	-	-	-	-	-	-	-	-
N	-	-	-	-	-	-	-	-	-
E	0.96	-	-	0.994	0.994	0.995	-	-	0.993
V	-	-	-	0.992	0.998	0.992	-	-	0.991
C	-	-	-	-	-	-	-	-	-
D	-	-	-	-	-	0.980	-	-	0.979
N	-	-	-	0.995	-	0.991	-	-	-
E	0.97	0.992	0.992	1.002	0.997	1.000	0.992	0.993	1.002
V	0.980	0.988	0.993	0.993	0.993	0.991	-	0.990	0.993
C	-	-	-	-	-	-	-	-	-
D	-	-	0.991	0.985	0.987	-	-	0.991	0.983
N	0.991	0.995	0.998	0.995	0.996	0.991	-	0.997	0.996
E	0.98	0.993	1.001	1.006	1.002	1.001	0.997	0.999	1.006
V	0.988	0.994	0.995	0.998	0.998	0.993	0.989	0.994	0.997
C	0.963	-	-	-	0.969	0.966	0.951	-	0.968
D	0.986	-	0.999	0.991	0.996	0.982	0.987	0.997	0.991
N	0.996	1.000	1.000	1.002	1.000	0.999	1.001	1.001	1.001

BALLISTIC DENSITY

Altitude = 50,000 ft

Station	Surface Density	0000 hr G.m.t.			1200 hr G.m.t.						
		W	S	F	W	S	F				
E	0.99	1.004	1.004	1.008	1.003	1.004	1.006	-	1.007	1.005	
V	0.996	0.999	1.000	1.004	1.000	0.995	1.000	-	1.003	0.998	
C	0.966	0.971	0.980	0.975	0.976	0.965	-	0.980	0.977	0.978	
D	0.990	0.995	1.002	0.999	1.001	0.990	0.996	1.004	0.999	1.000	
N	1.004	1.004	1.005	1.008	1.007	1.003	1.004	1.005	1.008	1.005	
E	1.00	1.010	1.009	-	1.012	1.010	1.012	1.009	-	1.009	1.010
V	1.000	1.004	-	1.006	1.002	0.998	1.004	-	1.008	1.002	
C	0.982	0.984	0.990	0.986	0.988	0.976	0.979	0.989	0.986	0.987	
D	0.997	1.003	1.007	1.005	1.005	1.000	1.002	1.006	1.003	1.002	
N	1.011	1.010	-	1.012	1.010	1.012	1.010	-	1.013	1.011	
E	1.01	1.016	1.015	-	-	1.016	1.016	1.014	-	-	1.013
V	1.006	1.008	-	-	1.007	1.003	1.009	-	-	-	1.005
C	0.988	0.991	0.995	0.993	0.993	0.988	0.989	0.996	0.994	0.996	
D	1.005	1.006	-	1.004	1.007	1.003	1.006	-	1.006	1.007	
N	1.016	-	-	-	1.017	1.017	1.017	-	-	-	1.017
E	1.02	1.019	-	-	-	1.020	-	-	-	-	1.016
V	1.009	1.014	-	-	1.011	1.008	1.013	-	-	-	1.009
C	0.995	0.998	1.002	1.000	0.999	0.997	0.998	1.003	1.001	1.001	
D	1.006	1.010	-	1.010	1.009	1.004	1.009	-	1.012	1.008	
N	-	-	-	-	-	-	-	-	-	-	

BALLISTIC DENSITY

Altitude = 50,000 ft

Station	Surface Density	0000 hr G.m.t.			1200 hr G.m.t.						
		W	S	SU	F	A	W	S	SU	F	A
E	1.03	-	-	-	-	-	-	-	-	-	1.023
V	-	-	-	-	-	-	-	-	-	-	-
C	1.000	1.007	1.005	1.008	1.007	1.003	1.006	1.004	1.008	1.004	1.004
D	1.010	1.015	-	1.016	1.011	1.009	1.015	-	1.014	1.011	-
N	-	-	-	-	-	-	-	-	-	-	-
E	1.04	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-
C	1.008	1.008	-	-	1.015	1.009	1.009	1.011	-	1.013	1.009
D	1.015	-	-	-	-	1.015	1.015	-	-	-	1.016
N	-	-	-	-	-	-	-	-	-	-	-
E	1.05	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-
C	1.019	1.015	-	-	-	1.018	1.016	1.016	-	-	1.017
D	1.023	-	-	-	-	1.023	1.024	-	-	-	1.023
N	-	-	-	-	-	-	-	-	-	-	-
E	1.06	-	-	-	-	-	-	-	-	-	-
V	-	-	-	-	-	-	-	-	-	-	-
C	-	-	-	-	-	-	-	-	-	-	-
D	-	-	-	-	-	-	-	-	-	-	-
N	-	-	-	-	-	-	-	-	-	-	-

TR 82-81

DISTRIBUTION

<u>Copies</u>		<u>Copies</u>	
Commander Naval Sea Systems Command Attn: SEA-62R SEA-62R42 SEA-62R3 SEA-62Y13C Library Washington, DC 20361	1 1 1 1 1	Commander Naval Avionics Center Indianapolis, IN 46216	1
Chief of Naval Material Washington, DC 20360	1	Commander Naval Coastal Systems Laboratory Panama City, FL 32401	1
Chief of Naval Operations Washington, DC 20350	1	Commanding Officer Naval Mine Engineering Facility Yorktown, VA 23691	1
Commander Naval Air Systems Command Attn: AIR-5411 AIR-5411C Library Washington, DC 20361	1 1 1	Commanding Officer Fleet Numerical Oceanography Center Monterey, CA 93940	1
Commander Naval Underwater Warfare Engineering Station Keyport, WA 98345	1	Naval Environmental Predication Research Facility Monterey, CA 95076	1
Director Naval Research Laboratory Washington, DC 20390	1	Commander Naval Ship Missile System Engineering Station Port Hueneme, CA 93043	1
Commanding Officer Naval Ordnance Station Indian Head, MD 20640	1	Commanding Officer Naval Ordnance Station Louisville, KY 40214	1
Commanding Officer Naval Weapons Support Center Attn: Code 5041 (J. Wildridge) Library Crane, IN 47522	1 1	Commander Naval Weapons Center Attn: Code 6224 Code 319 Library China Lake, CA 93555	1 2 3
Commander Naval Air Test Center Attn: SA-80 CS-31 (R. Nelson) SY-40 Patuxtent River, MD 20670	1 1 1	Commander Naval Air Development Center Warminster, PA 18974	1
		Commander Naval Oceans Systems Center San Diego, CA 92135	1

TR 82-81

DISTRIBUTION (Continued)

<u>Copies</u>	<u>Copies</u>		
Commander David W. Taylor Naval Ship Research and Development Center Bethesda, MD 20084	1	Commander Operational Test and Evaluation Force U.S. Naval Base Norfolk, VA 23511	1
Commander Pacific Missile Test Center Point Mugu, CA 93041	1	Commander Mine Warfare Command U.S. Naval Base Charleston, SC 29408	1
Commander Naval Underwater Systems Center Newport, RI 02480	1	Commanding Officer Naval Ocean Research and Development Activity NSTL Station, MS 39529	1
Commanding Officer Naval Weapons Evaluation Facility Kirtland Air Force Base Albuquerque, NM 87117	1	Armament Division Eglin Air Force Base, FL 32542	1
Commanding Officer Weapons Quality Engineering Center Naval Weapons Station Attn: WQEC/Code F32 Seal Beach, CA 91720	1	Armament Division Air Force Armament Laboratory Attn: DLYW Library Eglin Air Force Base, FL 32542	2
Superintendent Naval Postgraduate School Monterey, CA 93940	1	Aeronautical Systems Division Wright-Patterson Air Force Base, OH 45433	1
President Naval War College Newport, RI 02840	1	Air Force Weapons Laboratory Kirtland Air Force Base Albuquerque, NM 87117	1
Superintendent Naval Academy Annapolis, MD 21402	1	Air Force Flight Test Center Edwards Air Force Base, CA 93523	1
Center for Naval Analysis Arlington, VA 22209	1	Air Force Eastern Test Range Patrick Air Force Base, FL 32925	1
Strategic Analysis Support Group Applied Physics Laboratory Johns Hopkins University 8621 Georgia Avenue Silver Spring, MD 20910	1	Air Force Geophysics Laboratory Hanscom Air Force Base, MA 01731	1
		Superintendent U.S. Air Force Academy Colorado Springs, CO 80912	1

DISTRIBUTION (Continued)

<u>Copies</u>	<u>Copies</u>		
Air Force Weather Service Scott Air Force Base, IL 62226	1	Sandia National Laboratories P.O. Box 5800 Albuquerque, NM 87115	1
Air Force Western Test Range Vandenburg Air Force Base, CA 93437	1	Physical Science Laboratory New Mexico State University Box 3548 Attn: Stan Needham Las Cruces, NM 88001	1
Director U.S. Army Ballistics Research Laboratory Attn: AMXRD/BEL/FT Library Aberdeen Proving Ground, MD 21005	1	National Aeronautics and Space Agency Washington, DC 20546	1
Commander U.S. Army Armament Research and Development Command Dover, NJ 07801	1	National Bureau of Standards Washington, DC 20234	1
Commander White Sands Missile Range White Sands, NM 88002	1	Oklahoma State University Box 1925 Eglin Air Force Base, FL 32542	1
Commander U.S. Army Proving Ground Yuma, AZ 85364	1	National Climatic Center Federal Building Asheville, NC 28801	1
Commander U.S. Army Missile Research and Development Command Redstone Arsenal, AL 35809	1	Applied Physics Laboratory Johns Hopkins University 8621 Georgia Avenue Silver Spring, MD 20910	1
Commander U.S. Army Electronics Research and Development Command Fort Monmouth, NJ 07703	1	Defense Technical Information Center Cameron Station Alexandria, VA 22314	2
Atmospheric Science Laboratory U.S. Army Electronics Research and Development Command White Sands Missile Range White Sands, NM 88001	1	Library of Congress Attn: Gift and Exchange Division Washington, DC 20540	4
Sandia National Laboratories P.O. Box 969 Attn: Division 8152 (R. Everett) Library Livermore, CA 94550	1	Gidep Operations Office Corona, CA 91720	1
	1	NASA Scientific and Technical Information Facility P.O. Box 33 College Park, MD 20740	1

DISTRIBUTION (Continued)

<u>Copies</u>	<u>Local:</u>	<u>Copies</u>	
The Rand Corporation 1600 Main Street Santa Monica, CA 90406	1	E411	1
National Technical Information Service Springfield, VA 22151	1	K	1
Director Ordnance Research Laboratory Pennsylvania State University Box 30 State College, PA 16801	1	K10 K11 K40	1 25 5
University of Dayton Research Institute Dayton, OH 45409	1	K43 (Manrique)	1
National Weather Service 8060 13th Street Silver Spring, MD 20910	1	K44 (Masters) K50	1 5
Metropolitan State College 14th and Arapahoe Attn: Dr. W. A. Kemper (Box 69) Denver, CO 80203	1	G G10 G12 N20	1 1 10 1
Mr. Loren J. McAnelly 209 Walnut Drive Fredericksburg, VA 22405	1	N30 N50 N51 N52 N53 U	1 1 1 1 1 1
		E431	10

